# Constraints Analysis 

## for

# Three Bridges in Nogales, AZ: Gold Hill Road, Produce Row, and Calle Sonora 

## Project Number: 15-12913



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### 1.0 Introduction

City of Nogales Project No: 15-12913
Project Title: Constraints Analysis for Three Bridges in Nogales, AZ: Gold Hill Road, Produce Row, and Calle Sonora

The constraints analysis document has been prepared to determine if improvements can be made to three (3) side streets east of Grand Avenue (B-19): Gold Hill Road, Produce Row and Calle Sonora. This study evaluated the feasibility to realigning the roadway to meet horizontal curvature standards, adding capacity to accommodate future traffic, improving turning movements, and replacing the bridges over the Nogales Wash with a structure designed to accommodate the overweight truck traffic design load all while not adversely impacting floodplain elevations, accommodating utilities, and meeting Union Pacific Railroad and ADOT standards for design and signalization. The State Map and Project Vicinity Map are located in Figure 1 and Figure 2.

The project consists of three side street segments along Grand Avenue (B-19). Project exhibits are located in Appendix A.

## Calle Sonora

The Calle Sonora segment begins at the Grand Avenue east curb line and continues east to Smokey Lane. The segment then continues southward along Hohokam Drive approximately 600 feet. The reconstruction along Calle Sonora includes eastbound and westbound travel lanes with curb, gutter and sidewalk, a concrete median to provide driveway access control, a one-way center left turn lane, a right turn bay to northbound Grand Avenue and replacement of the bridge over Nogales Wash. Hohokam Drive will be realigned approximately 300 feet to the east to incorporate a one-way loop connection to Smokey Lane which will divert the turning vehicles causing queues on Calle Sonora.

## Produce Row

The Produce Row segment begins at the Grand Avenue east curb line and continues east to Donna Avenue. The reconstruction along Produce Row includes eastbound and westbound travel lanes with 6 foot shoulders, a one-way center left turn lane, and replacement of the bridge over Nogales Wash.

## Gold Hill Road

The Gold Hill Road segment begins 300 feet west of Grand Avenue on Mesa Verde Road and continues east along Gold Hill Road, terminating 400 feet east of Palenque Avenue. The reconstruction along Mesa Verde Road includes eastbound and westbound travel lanes with curb, gutter and sidewalk, a one-way center left turn lane, and driveway relocations. The reconstruction along Gold Hill Road includes eastbound and westbound travel lanes with curb and gutter, a one-way center left turn lane, replacement of the bridge over Nogales Wash and geometric
realignment east of the railroad tracks. The purpose of the realignment is to remove the 90 degree turn (horizontal curve) and improve safety at the Silver Hill Drive intersection.

The roadway and structure needs will require additional right-of-way and easements. Right-of-way shown in exhibits is based on GIS data. Survey will be required during final design to determine needs and acquisition.

The total estimated cost for this project is $\$ 11,200,000$. This cost reflects project construction, design and right-of-way costs. Environmental clearance is not included. A breakdown of the costs is as follows:

## Calle Sonora

| Construction Cost | $\$ 3,070,000$ |
| :--- | :--- |
| Design Cost | $\$ 405,000$ |
| Right-of-Way | $\$ 700,000$ |
| Total Project Cost | $\$ 4,800,000$ |

## Produce Row

Construction Cost $\$ 1,720,000$
Design Cost $\$ 230,000$
Right-of-Way $\$ 158,000$
Total Project Cost $\$ 2,500,000$
Gold Hill Road
Construction Cost $\quad \$ 2,800,000$
Design Cost $\quad \$ 369,000$
Right-of-Way \$179,000
Total Project Cost $\$ 3,900,000$
These conceptual designs are preliminary and have not addressed all design issues such as minimizing impacts to neighboring properties and incorporating feedback from stakeholders. Final design will follow a process whereby many of these design details will be addressed and presented to City Staff at multiple design stages to demonstrate how concerns are being incorporated. No funds have currently been allocated for the project; however, the City has overweight permit fees that can be applied toward both final design and construction. An itemized cost estimate is provided in Figure 7.

Figure 1. State Map


Figure 2. Project Vicinity Map


Figure 3. Project Location Map


### 2.0 Background Data

The purpose of this project is to provide a conceptual design for replacing the Nogales Wash bridges that accommodates the heavier truck loads presently being permitted by ADOT. Due the age of the existing bridges, no as-builts have been
located and their design loads are unknown. Replacement of the bridges is the only realistic option to ensure that the structural integrity is provided to service the heavier truck loads. The secondary purpose of the project is to identify roadway configurations that improve mobility and safety within the short distances constrained by Grand Avenue, the railroad and the existing bridges. Preliminary traffic analysis has recommended geometric improvements consisting of a center turn lane to reduce vehicle queuing and increase efficiency of the intersections.

One of the major issues on this project is the existing bridge width. With the amount of large truck traffic in this area, the width restriction creates a "bottle neck" which is further complicated with the close proximity to the railroad tracks. Width of bridge also has implications on the turning templates of large trucks as is evidenced in the field, trucks have hit bridge barriers while trying to navigate the smaller radii and avoid oncoming traffic.

This study will document that improvements proposed at the three bridges are unable to solve the regional and international flooding issue with the Nogales Wash. The solutions proposed are limited to no rise in water surface elevation and may not exacerbate flooding conditions on neighboring properties.

### 3.0 Project Description and Scope

The project includes evaluation of the reconstruction of the bridges over the Nogales Wash and the associated roadway approaches at Calle Sonora, Produce Row and Gold Hill Road. Site specific improvements area are outlined below.

## Calle Sonora

The existing 30 -foot wide bridge and roadway will be removed and a new bridge consisting of a 12 -foot wide westbound travel lane, a 14 -foot wide eastbound travel lane, a 12 -foot wide left turn lane, a 4 -foot center median and 6 -foot shoulders in each direction will be constructed. The roadway connection to Grand Avenue will be reconstructed to include a westbound right turn, through and left turn lanes, an eastbound through lane and a concrete median for railroad gate equipment and driveway access control. The railroad crossing will require upgrades to accommodate this wider configuration. Hohokam Drive will be relocated 270-feet to the east and a one-way loop will be incorporated immediately to the east of the bridge to re-direct traffic accessing Smokey Lane. The purpose of this loop or "jug handle" is to remove the queuing encountered with turning vehicles between the railroad and Smokey Lane. The roadway profile between the railroad tracks and the bridge will be adjusted to reduce the abrupt elevation change as vehicles approach the track pad. Final design analysis may indicate the need to reconfigure or relocate the parking area at the northeast corner of Smokey Lane and Calle Sonora.

## Calle Sonora Alternate Route

An alternative to the proposed improvements to the east of the bridge is described in the Road Safety Assessment of Mariposa Road (SR 189)/Target Range Road and Calle Sonora/Hohokam Drive prepared by ADOT in June 2009. This alternative recommends converting Smokey Lane to one-way southbound and acquiring property on the north side of the Villa's Food Market to use to access Smokey Lane from North Ocean Garden Drive.

## Calle Sonora Roundabout

An alternative to the "jug handle" is a more traditional roundabout, which serves the same purpose of circulation as the jug handle but without the stop conditions. A single-lane roundabout was laid out with a 130' inside diameter which accommodates a WB-67 (interstate semi-trailer) design vehicle. The roundabout geometry represents the paved footprint without curb and sidewalk. The roundabout, as laid out, may have some slight encroachment into private property on the north but was done as an exercise to show the feasibility. Refinements to the geometry of the roundabout could be evaluated in advanced planning or final design to try to limit acquisition of property north of Calle Sonora and also to accommodate driveway access.

## Produce Row

The existing 30 -foot wide bridge and roadway will be removed and a new bridge consisting of a 12 -foot wide westbound travel lane, a 12 -foot wide eastbound travel lane, a 12 -foot wide left turn lane, and 6 -foot shoulders in each direction will be constructed. The roadway connection to Grand Avenue will be reconstructed to include a westbound through lane, a westbound left turn lane and an eastbound through lane to match the lane configuration to the west of Grand Avenue (Frank Reed Road). The roadway profile between the railroad tracks and the bridge will be adjusted to reduce the abrupt elevation change as vehicles approach the track pad.

## Gold Hill Road

The existing 30 -foot wide bridge and roadway will be removed and a new bridge consisting of a 12 -foot wide westbound travel lane, a 12 -foot wide eastbound travel lane, a 12 -foot wide left turn lane, and 6 -foot shoulders in each direction will be constructed. The roadway connection to Grand Avenue will be reconstructed to include a westbound through lane, a westbound left turn lane and an eastbound through lane. Mesa Verde Road (west connection of Grand Avenue) will also be reconstructed with a similar roadway configuration. The Mesa Verde Road profile will not be adjusted to improve sight distance or to provide a more desirable approach grade to the intersection due to stormwater recommendations. Gold Hill Road will be realigned from N. Silver Hill Drive approximately 600-feet east. The purpose of the realignment is to reduce the conflict points at the N. Silver Hill Drive and Gold Hill Road intersection and to remove the 90 -degree horizontal curve on Gold Hill Road immediately south of this intersection. In addition, this will provide
a more defined access to Palenque Avenue, as current traffic encroaches onto the adjacent private property to travel southbound. These roadway geometric improvements will require new right-of-way and easements.

In scoping meetings the City had requested to investigate whether northbound right turn lanes on Grand Ave would provide vehicle storage during train crossing for those vehicle desiring to turn right onto the subject project side streets, thus freeing up the eastern northbound through lane. Evaluation of this request reveals that utilities and city bus pads are constraining the geometry from being able to fit another lane in along Grand Ave.

No funds have currently been allocated for the project. An itemized cost estimate is shown in Figures 6, 7 and 8.

The project will require relocations of overhead power poles, valve adjustments, sanitary sewer manhole adjustments, and the relocation or adjustment of gas facilities due to bridge reconstruction. Utility relocations are anticipated to the west of the intersection of Gold Hill Road and Palenque Avenue due to the realignment of Gold Hill Road.

Section 8 shows a recommended action item checklist for the project.

### 4.0 Project Development Considerations

### 4.1.1 Environmental Overview

The intent of this project is to improve mobility, safety and intersection efficiency at Gold Hill Road, Produce Row and Calle Sonora east of Grand Avenue (B-19). The project improvements will require acquisition of new right-of-way.

The following sections summarize the environmental issues and the additional analysis and documentation that would be undertaken if federal construction funding is used.

### 4.1.2 Biology

It is anticipated that a Biological Evaluation (BE) will be required as a condition of using a USACE Nationwide Permit. A qualified biologist would conduct a site visit to evaluate the potential for the project to affect federally listed threatened and endangered species, as well as AGFD special status species. Preparation of the BE would include another review and evaluation of USFWS species lists for Santa Cruz County, as well as the AGFD review tool, if required.

### 4.1.3 Cultural Resources

It is anticipated that a Class 3 archeological inventory survey will be required as a condition of using a USACE Nationwide Permit.

### 4.1.4 Clean Water Act

The Nogales Wash is a Water of the U.S. (WOUS) that is regulated by the Corps of Engineers Regulatory Branch. Any fill of dredged or discharged material will require a Section 404 Permit. Based on anticipated disturbance quantity we assume that the project(s) will qualify for a Nationwide Permit (NWP). Steps for compliance with Section 404 of the Clean Water Act are as follows:

- Confirm whether a Jurisdictional Delineation (JD) exists for the Nogales Wash or prepare a Preliminary Jurisdictional Delineation (PJD)
- Conduct impact calculations of WOUS in total acreage
- Determine if amount of impacts meets NWP threshold or whether Individual Permit process must be followed.
- Prepare BE and scoping letter with US Fish and Wildlife Service
- Prepare Type III Cultural Resources Survey
- Prepare Pre-construction Notification

Since the Nogales Wash is an impaired WOUS it will have additional conditions during the Section 401 Certification. The Nogales Wash is impaired with Ammonia (2004), chlorine (1996), Copper (dissolved) (2004), and E. coli (1998). It is noted that Nogales Wash is a mostly perennial water source and if wetland features are observed, the act of de-watering during construction may be regulated to a certain season and time-frame.

### 4.1.5 100-Year Floodplains

The project limits are within Federal Emergency Management Agency Flood Insurance Rate Maps (FIRM) 04023C0464C, and 04023C0631C, which are both dated December 2, 2011 (See Figure 4, Floodplain Exhibit). According to the FIRM the project area is within Zone AE of the 100 -year floodplain. Proposed structures are not expected to adversely impact base flood elevations. A hydraulic analysis was conducted using the Effective Flood Insurance Study HEC-RAS model with modifications including showing the new bridges. Results of the hydraulic analysis were compared to the existing base flood elevations (BFEs) and it was determined that the proposed improvements will not increase BFEs as a result of the new structures. Models and results are presented in the Appendix

Figure 4, Floodplain Exhibit


### 4.1.6 National Pollutant Discharge Elimination System

It is expected that project construction would disturb 1 or more acres of land; therefore, a Storm Water Pollution Prevention Plan would be prepared and a Notice of Intent would be filed with Arizona Department of Environmental Quality (ADEQ) in accordance with Arizona Pollution Discharge Elimination System (AZPDES) regulations. ADEQ has identified the project reach as an "impaired" water way.

### 4.1.7 Scenic or Historic Routes

No scenic or historic routes are within the project limits.

### 4.1.8 Temporary Construction Impacts

Temporary construction easements on adjacent lands will be required. Detours would be provided for pedestrians and mitigation measures would be developed to minimize impacts on traffic and pedestrians during construction. Site specific construction phasing and detours outlined below.

## Calle Sonora

During the demolition of the existing bridge and construction of the new bridge and approaches, traffic would be detoured to the Doe Street bridge which is approximately one mile south.

## Produce Row

Reconstruction of the bridge structure will require two phases. The first phase consists of detouring traffic to the south half with alternating movements with flaggers and reconstructing the north half. During the second phase of work, traffic would utilize the completed portion while reconstruction shifted to the south half.

## Gold Hill Road

During the demolition of the existing bridge and construction of the new bridge and approaches, traffic would be detoured 0.9 miles east on Gold Gill Road, 3.5 miles south on Camino Vista del Cielo/Old Patagonia Road and 1.6 miles west on SR 82 to the Patagonia Highway bridge at Grand Avenue. The total detour route is approximately 6 miles. Phasing the bridge reconstruction would not allow for vehicle storage west of the bridge due to the close proximity to Grand Avenue but is noted to be a second option.

### 4.1.9 Public and Agency Involvement

During preparation of the CE, scoping letters would be distributed to pertinent agencies, stakeholders, and adjacent landowners. The letters would describe the project and solicit comments. Due to the impacts on traffic during construction, a public meeting is anticipated for the project.

### 4.2 Construction Contract Method

This project is anticipated to be a Design-Bid-Build contract.

### 4.3 Drainage and Geotechnical Requirements

### 4.3.1 Existing Drainage Characteristics

The project consists of evaluating three proposed bridges for possible replacement along the Nogales Wash, which were modeled as part of a detailed study for the Flood Insurance Study effective December 2, 2011. The Nogales Wash channel lacks capacity and overbank flow is common. The existing bridges at Gold Hill Rd, Produce Row, and Calle Sonora would all be overtopped during the 100-year design storm. Additionally, evidence of lateral erosion is present on the eastern channel bank, upstream of Produce Row.

### 4.3.2 Drainage Structure Requirements

Proposed project improvements include three bridge replacements and improved bridge approaches. The bridge at Produce Row is proposed to be extended 20 feet on the east side to account for channel widening and to increase hydraulic efficiency. The effective HEC-RAS model was provided by Santa Cruz County to model the impacts of the proposed improvements. The effective model was revised to more accurately model existing roadway geometry.

Recommended bridge types were selected to prevent rise in water surface elevation and maximize conveyance and were evaluated relative to the revised, Effective Nogales Wash HEC-RAS model. Infrastructure improvements were designed to prevent adverse impacts, defined as no increase in water surface elevation. Proposed water way cross-sectional area is increasing from existing conditions and abutments will be vertical wall abutments which will transition back to existing channel width by the use of concrete lined bank transitions. See Table 1 for bridge recommendations and a comparison of water surface elevations. Location of project improvements and hydraulic cross sections (for reference to HEC-RAS model) are shown on Figure 5, Hydraulic Exhibit.

New bridge structures will not be able to solve the regional flooding problem. Presently there is not enough capacity in the channel which is sandwiched between the railroad and Grand Ave. As the Floodplain Exhibit on page 9 shows, Grand Avenue and significant extents of commercial and residential property along the corridor will continue to be in a FEMA special flood hazard area after these projects are implemented.


## Kimley»"Horn

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| 0 | 500 | 1,000 | 2,000 |  |
| :--- | :--- | :--- | :--- | :---: |
|  |  |  |  |  |
|  | Feet |  |  |  |

Figure 5, Hydraulic Exhibit

Gold Hill Road, Produce Row and Calle Sonora

Table 1. Bridge Hydraulics

| Location | Bridge Type | Superstructure <br> Depth <br> [ft] | \# of <br> piers | Upstream WSEL <br> [ft] | Delta <br> WSEL <br> [ft] |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Calle <br> Sonora | Existing Conditions | 1.50 | 1 | 3750.25 | -- |
| Calle <br> Sonora | Proposed Box Beam | 2.67 | 1 | 3750.15 | -0.10 |
| Produce <br> Row | Existing Conditions | 3.70 | 0 | 3709.45 | -- |
| Produce <br> Row | Proposed AASHTO Type II | 4.00 | 0 | 3708.83 | -0.62 |
| Gold Hill | Existing Conditions | 3.50 | 2 | 3687.57 | -- |
| Gold Hill | Proposed Box Beam | 3.17 | 0 | 3687.36 | -0.21 |

## Scour Calculations

Scour calculations were performed according to the methodology outlined in the City of Tucson's Standards Manual for Drainage Design and Floodplain Management. Scour calculations were completed based on hydraulic conditions in Nogales Wash improvements. Scour components include Long Term, Local, General, Anti-Dune, Low-Flow Thalweg. The local scour component includes only pier scour. The Nogales Wash channel has a slope that appears to be stable at $0.8 \%$. Based on this profile, the long term scour baseline is approximately 3 feet below grade at Produce Row suggesting that some degradation could occur within that reach. Gold Hill Rd and Calle Sonora are already below the long term scour profile. Refer to Table 2 for scour depth recommendations. Table 2, Scour Design Recommendations gives design scour depths which are based on the worst case of the 10 -year or 100 -year. Since the general scour component is based on the relationship between channel depth and velocity, the 10-year event, in some cases, is more severe. Scour calculations are provided in Appendix C, Drainage Support.

Table 2. Scour Design Recommendations

| Proposed Improvement | Design Scour <br> Depth for Pier <br> (ft) | Design Scour Depth <br> for <br> Abutment/Channel <br> Protection <br> [ft] |
| :---: | :---: | :---: |
| Gold Hill Rd Box Beam Bridge | N/A | 7 |
| Produce Row AASHTO II Bridge | N/A | 9 |
| Calle Sonora Box Beam Bridge | 23 | 10 |

### 4.3.3 Geotechnical Requirements

A geotechnical report was not completed for this project assessment. The preliminary design roadway pavement section will assume 6" Asphalt Concrete over 6" Aggregate Base Course. This pavement section was used on the recently designed Intersection project in Santa Cruz County. A geotechnical report will be required for final design to address pavement recommendations, structure foundation data, channel bank slope recommendations and earthwork.

### 4.4 Critical Outside Agency Involvement

The City of Nogales is responsible for public and agency scoping activities which include providing a description of the project's scope of work and a schedule to local residents and businesses as well as adjacent local, county, and state agencies. Agencies and the public will be given an opportunity to comment on the project and the City of Nogales will respond to any comments.

A meeting was held March 13, 2015 with the ADOT Tucson District traffic team to discuss ADOT requirements and coordination. To obtain ADOT approval to modify a connection to their highway system, the design team will be required to submit a set of plans and a drainage report. To perform construction work within ADOT right-of-way, an encroachment permit will be needed. This permit also requires an environmental certification.

Initial contact with Union Pacific Railroad was initiated in March 2015. E-mail correspondence is summarized below:
-Designers need to consider standards regarding crossings (AREMA) and the limiting conditions to the west of the railroad.
-Grand Avenue (Old Nogales Hwy) is close to the railroad and the approaches to these crossings and intersections require a creative, well documented approach to both traffic and train warning signal installation and interconnection.

### 4.5 Right-of-Way Requirements

The right-of-way corridor within the project limits varies as follows:

| Grand Avenue | ADOT R/W Width <br> (FT) | UPRR R/W Width <br> (FT) |
| :---: | :---: | :---: |
| Calle Sonora | 120 | 46 |
| Produce Row | 102 | 88 |
| Gold Hill Road | 160 | 200 |

Note: Dimensions based on as-builts and need to be confirmed with agency right-of-way departments. The contractor will be required to obtain a Right-of-Entry Agreement from UPRR.

| City <br> Street | City of Nogales <br> R/W Width <br> (FT) | New R/W Acquisition and Easements <br> (APN \# and description) |
| :---: | :---: | :--- |
| Calle <br> Sonora | 50 to 70 | New R/W: 10201008A (full take), <br> 10201013 (partial), 10201009 (partial), <br> 10201014 (partial), 10201075 (partial) |
| Hohokam <br> Drive | 55 to 75 | New R/W: 1020121086 (partial) |$|$| Produce <br> Row | 60 |
| :---: | :--- |
| New R/W: 10528016 (partial), 10528005A <br> (partial), 10528012A (partial), 10528005B <br> (partial) <br> TCE: 10528016 (at north driveay), <br> Road <br> (at bridge) | 85 |
| Gold Hill <br> Road <br> (at <br> realignment) | 60 |
| Extend public easement though UPRR right- <br> of-way |  |
| Mesa <br> Verde <br> Road | New R/W: 10502004A (partial) <br> Slope Easement: 10502004A (north fill <br> slope) <br> TCE: 1052018 (Palenque Ave), 1052014B <br> (Palenque Ave) |

Note: Dimensions based on GIS data and need to be confirmed with agency right-of-way departments.

Due to the changing conditions of land use and development, it is recommended to proceed with the right-of-way process to reserve areas needed for these improvements.

### 4.6 Utility Relocation Requirements

A Blue Stake Design Ticket was submitted on February 16, 2015 to identify utility companies which have facilities within the proposed construction limits.

The following are the companies that have facilities within the area, their contact representative and references to requirements or responses.
ADOT-Tucson District
Jim Lewis
Drainage
(520) 604-0372

ADOT has drainage facilities along Grand Avenue at Gold Hill Road. Widening may require drainage ditch reconstruction and culvert extensions.

ADOT-Tucson District
Anthony Barcelo
Rdwy Lighting and Traffic Signals (520) 838-2842
ADOT owns and maintains roadway lighting and traffic signals at all three traffic intersections. Existing traffic signals will need to be removed and replaced to accommodate cross street widening.

| City of Nogales | Lee Jacobs, PE |
| :--- | :--- |
| Sewer and Water | (520) 287-8352 |

The City of Nogales owns and operates a 16 inch water main and a 30 inch sanitary sewer pipe along the east bank of the Nogales Wash. Utility modifications should be limited to water valve and manhole adjustments at Calle Sonora. Produce Row modifications will include backflow assembly, water meter and fire hydrant relocation along with meter valve adjustments. A private PVC water line is attached to the south side of the Produce Row bridge which will require relocation during reconstruction. A significant above ground water facility located 200 feet east of the railroad at Gold Hill Road will need to be relocated due to the new roadway realignment. Water valve and meter work may also be required.

$$
\begin{array}{ll}
\text { CenturyLink } & \text { Robert Porter } \\
\text { Coaxial and Fiber } & \text { (520) 281-0153 }
\end{array}
$$

CenturyLink has underground and overhead facilities along Calle Sonora that will require relocation. There are underground lines located at the south end of the Produce Row bridge that require further locating methods to determine conflicts. Underground lines are also located along the existing north curb line of Gold Hill Road that will do not appear to be in conflict at this time.

## Conterra Ultra Broadband

Hector Soberon
Communication and Fiber
(800) 634-1374

Facilities are located along the west side of Grand Avenue at Gold Hill Road and Produce Row. No conflicts are anticipated at this time.

| MediaCom | Kevin Young |
| :--- | :--- |
| Coaxial and Fiber | (602) 295-5213 |

MediaCom has overhead facilities on the power poles along Calle Sonora and Produce Row that will require relocation to accommodate roadway widening. Overhead facilities are also on the power poles along the west side of Grand Avenue at Gold Hill Road that are not anticipated to be in conflict.

UniSource Energy Services
Electrical and Gas

Carlos Parra
(520) 755-7950

UniSource owns overhead power facilities that run along the west side of Grand Avenue at all three intersections. Conflicts are not anticipated for this facility. Overhead power is also located along the north side of Calle Sonora, west side of Hohokam Drive, south side of Produce Row and the south side of Gold Hill Road. Relocation is anticipated at Calle Sonora and Produce Row to accommodate roadway widening.

UniSource owns and operates natural gas pipelines that are attached to all three bridges that will require further coordination and relocation. Cost for relocation was not considered assuming license agreements exists for use of City Right of Way.
Valley Telephone Cooperative
Danny Chastain
Coaxial and Fiber
(520) 384-2231

Arriba fiber is buried inside UPRR right-of-way north of Gold Hill Road to Doe Street (one mile south of Calle Sonora). Conflicts are not anticipated at this time.

Costs for utility relocation work within the project estimates is limited to City owned utilities. Costs for private utility relocation is assumed to be paid for by the owner of the utility.

### 4.7 Traffic Requirements

A traffic evaluation was performed to determine and evaluate existing conditions. A future traffic forecast was conducted based on growth trends and feedback from members of the Fresh Produce of the Americas (FPAA). The interviews provided a local perspective of the existing conditions and also assisted with determining what the future needs in terms of traffic growth require. The complete traffic evaluation can be found in Appendix B.

Traffic data was collected on February $4^{\text {th }}, 2015$. The traffic data was collected during what would be considered the peak season for produce shipments from Mexico. The collected traffic data includes 24 -hour tube counts located on the 3 bridges and AM/PM peak period intersection turning movement counts. Turning movement counts were collected at the intersections of Grand Avenue / Gold Hill Road, Grand Avenue / Produce Row, Grand Avenue / Calle Sonora, Calle Sonora / Smokey Lane. Also, a vehicle classification study was performed concurrently with the 24-hour tube counts to provide truck percentage that would typically occur.

## Roadway-Bridge Cross-section

Both safety and traffic operational concerns due to the continuous heavy truck traffic require the need for a wider cross-section at the three locations. According to field observations and feedback from FPAA members, trucks turning from cross-
streets must overtake opposing lanes. Thus, interrupting opposing traffic which causes vehicles to queue up or increase unsafe situations that may lead to collisions.

To accommodate the heavy trucks turning from access drives or intersecting roadways, it is recommended to increase the roadway cross-section. The increased cross-section shall allow heavy trucks to execute turning maneuvers without utilizing the opposing lane. It is recommended that each of the three roadways consist of wider through lanes. Also, include a left-turn lane on the westbound approaches such that the storage length is extended east of the bridges as engineering constraints permit.

## Turn Lane Warrant

Turn Lane Warrants from the ADOT Traffic Engineering Policies, Guidelines, and Procedures (December 2014), Section 200, were utilized to determine the need for right-turn lanes on the northbound approaches of each of the three intersections along Grand Avenue. Existing and future traffic volumes justify the need for rightturn lanes at the 3 northbound approaches. However, due to the observed engineering constraints, such as right-of-way, utilities and bridge constraints, constructing right-turn lanes along Grand Avenue lanes would be infeasible.

## Intersection Operations

To improve intersection operations to accommodate the estimated future traffic volumes, it is recommended to implement the following concurrently with the construction of the new bridges:

## Calle Sonora

- Construct an exclusive right-turn lane on the westbound approach of Calle Sonora, designed such that it meets ADOT minimum standards.
- With the exclusive westbound left-turn lane, reconfigure the traffic control signal for optimized standard phasing. Thus, removing the existing split-phasing as it would not be necessary with the enhanced intersection configuration would allow for efficient shorter cycle lengths.


## Produce Row

- Reconfigure the traffic control signal's cycle length to allow for turning trucks completely clear the intersection during approaches green phase. Comments from the stakeholder interviews and observations shows that existing timing of the signal phases, yellow change and red clearance intervals, especially right/left turning trucks, doesn't allow trucks to safely clear out of the intersection. Note that there is no standard practice or methods recommended for intersections with significant heavy truck percentages.


## Gold Hill Road

- It is recommended to construct an exclusive left-turn lane at the eastbound approach of Mesa Verde Road, designed such that it meets ADOT minimum standards. With the left-turn lane on the westbound approach as part of the Gold Hill Road enhancement, construction of the eastbound dedicated left-turn lane would not require split-phasing. Thus, reduce delays of the left/right turning vehicles during the peak periods.


## Access Management

The potential reconstruction of the 3 bridges and roadways, would allow for an opportunity to implement access management practices on each roadway. Access management allows for maintaining roadway safety and mobility by controlling access location, design, spacing and operation. The following is recommended to be implemented during the construction of the new bridges:

- At Calle Sonora, close 1 of the northbound driveways (Alex's Tires, Inc.) and relocate the southbound and northbound driveways, located west of the bridge. Relocate the access drives from the intersection of Grand Avenue / Calle Sonora to allow 150' minimum spacing between the access drives and the Grand Avenue curb line. A 150 ' minimum is typically a standard policy in many jurisdictions.
- Also, access drive turning restriction should be considered at the relocated driveways along Calle Sonora for both the north and south access drives due to the proximity to the signalized intersection. Allowing all movements may increase accident potential. Thus, consider a roadway cross-section that would restrict left-in and left-out movements on both driveways.
- At Produce Row, construct an access drive for the two businesses on the north and south of Produce Row, west of the bridge. Locate the dedicated access drives such that at a minimum 150' spacing or more exists between the access drive and the Grand Avenue curb line.
- With the construction of the eastbound exclusive left-turn lane on Mesa Verde Road, construct new access drives for both the north and south properties. Construct such that a minimum 150 ' spacing or more exists between the access drive and the Grand Avenue curb line.


### 4.8 Seasonal Considerations

Due to anticipated conflicts with UniSource electrical and gas facilities, the schedule for utility relocations will need to account for the "peak use" timeframes for electric and gas. The general peak seasons are the following:

- Electric Power: April - October
- Gas: October - March

The relocation of large steel power poles and gas pipelines require significant lead time. This timeframe must also be accounted for in the project schedule. Fiber optic lines are often relocated along with the electric lines. Water modifications are performed in the off peak season between October 1 and March 30. Sewer facilities general have no seasonal constraints.

Nesting season for migratory birds may preclude removal of vegetation as a condition of utilizing a Nationwide Permit from the Corps. The Biological Evaluation would set target dates for when these periods occur and the requirements for working around trees with nesting sites.

### 4.9 Design Criteria

The project will be implemented in accordance with A Policy on Geometric Design of Highways and Streets (2011), Pima County/City of Tucson Pavement Marking Design Manual (2008), and the latest edition of the Arizona Department of Transportation standard drawings, specifications and design guidelines.

No AASHTO design exceptions apply to this project.
Side street and driveway turning movements have been checked for lane encroachment using a WB-50 design vehicle per ADOT RDG Table 407.2. Intersection sight distance at these locations have also been checked per AASHTO sight triangle methods. Preliminary analysis indicates a sight obstruction from the bridge barrier for the north driveway on Calle Sonora between the railroad and the bridge. Further design will be required to address this driveway and adjacent parcel configuration.

Access control will be implemented in the form of a concrete median on Calle Sonora between Grand Avenue and Smokey lane. This is recommended to remove the queuing caused by stopped vehicles waiting to turn across traffic lanes to the adjacent driveways. Access control to Palenque Avenue will also be improved by using curb and gutter to provide defined southbound direction.

Geometric layouts presented in the appendix are preliminary and further traffic analysis is warranted at the final design stage to confirm the proposed layouts will work with updated movements and traffic counts.

### 4.10 Structural Design

As noted in the previous sections, the proposed roadway improvements to Gold Hill Road, Produce Row and Calle Sonora require improvements to the existing bridges over the Nogales Wash on these side streets. For the purpose of this report it is assumed that the bridge improvements will consist of full bridge replacements. The bridge improvements include both vertical and horizontal geometric and structural improvements. The increased roadway widths at the bridge locations require wider structures in addition to the roadway profile modifications requiring adjustments to the existing bridge profiles. These side streets see significant overweight truck traffic and therefore in addition to the AASHTO HL-93 live loading requirements, the bridges will be designed for to accommodate an overweight truck loading of 90,000 pounds. Utilities supported on the existing bridges will need to be considered during final design. ADOT has a policy of not allowing utilities on new bridges, but since the funding source for construction will likely be local funds the City can decide. Cost for utility relocation was not considered assuming that the City has active license agreements with the utilities for use of City Right of Way.

### 4.10.1 Calle Sonora

## Existing Bridge

The existing bridge is a two-span precast prestressed concrete box beam bridge with an overall bridge length of approximately $70-\mathrm{ft}$ and overall bridge width of approximately $36-\mathrm{ft}$. As-builts for the bridge were not available, but based on information gathered and recent ADOT Bridge Inspection Reports it is assumed that the existing bridge is supported on drilled shaft foundations at the abutments and pier. This bridge has not been identified as scour critical.

There is an existing gas line and underground telephone line supported on the north side of the bridge that will be relocated to the new bridge structure.

## Proposed Improvements

The proposed bridge improvements will replace the existing bridge in kind with improved geometrics to match the roadway widening and adjusted roadway profile.

The proposed bridge geometry will consist of a 12 -foot wide westbound travel lane, a 14 -foot wide eastbound travel lane, a 12 -foot wide left turn lane, a 4 -foot center median, 6 -foot shoulders in each direction and 5 '-10" sidewalk with ADOT Combination Pedestrian Traffic Barrier Railing in each direction for an overall bridge width of $70-\mathrm{ft}$. The overall bridge length will $70.5-\mathrm{ft}$. The bridge profile will be raised slightly from the existing bridge profile to match the proposed roadway improvements.

As discussed in the Drainage section, the existing creek bottom will be excavated out below the bridge to mitigate effects of the proposed roadway and bridge
improvements on the current floodplain elevation. The bridge will abutments will be full height abutments supported on drilled shafts. The bridge pier will also be supported on drilled shafts. The existing wash banks on the inlet and outlet of the bridge will be protected with slope protection as discussed in the Drainage section.

### 4.10.2 Produce Row

Existing Bridge
The existing bridge is a single span steel I-beam bridge with an overall bridge length of approximately $41-\mathrm{ft}$ and overall bridge width of approximately $29.5-\mathrm{ft}$. As-builts for the bridge were not available, but based on information gathered and recent ADOT Bridge Inspection Reports it is assumed that the existing bridge is supported by full height abutments on spread footings. The 2013 ADOT Structure Inventory and Appraisal report classifies the bridge as scour critical.

There is an existing gas line supported on the north side of the bridge that will be relocated to the new bridge structure. There is also an existing private 2" PVC water line on the south side of the bridge that will be relocated to the new bridge structure.

## Proposed Improvements

As discussed in the Drainage section, an increased bridge span is required at this location due to existing bank erosion issues and to improve flow in the wash and mitigate effects of the proposed roadway improvements on the current floodplain elevation. Based on the increased span length and desire to minimize the overall depth of the bridge structure, the proposed bridge will consist of a single span precast prestressed AASHTO box beam bridge with full height abutments.

The proposed bridge geometry will consist of a 12 -foot wide westbound travel lane, a 12 -foot wide eastbound travel lane, a 12 -foot wide left turn lane, 6 -foot shoulders in each direction and $5^{\prime}-10^{\prime \prime}$ sidewalk with ADOT Combination Pedestrian Traffic Barrier Railing in each direction for an overall bridge width of $62-\mathrm{ft}$. The overall bridge length will $60-\mathrm{ft}$. The bridge profile will be raised slightly from the existing bridge profile to match the proposed roadway improvements.

The bridge abutments will be full height abutments supported on drilled shafts. The existing wash banks on the inlet and outlet of the bridge will be protected with slope protection as discussed in the Drainage section.

### 4.10.3 Gold Hill Road

Existing Bridge
The existing bridge is a three-span cast-in-place concrete closed frame slab bridge with an overall bridge length of approximately $70-\mathrm{ft}$ and overall bridge width of $33.3-\mathrm{ft}$. As-builts for the bridge were not available, but based on information gathered and recent ADOT Bridge Inspection Reports it is assumed that the existing
bridge is supported on spread footings protected by a concrete slab scour floor. This bridge has not been identified as scour critical.

There is an existing gas line and underground telephone line supported on the south side of the bridge that will be relocated to the new bridge structure.

## Proposed Improvements

Two bridge types, a three-span cast-in-place concrete closed frame slab bridge and a single span precast prestressed AASHTO box beam bridge with full height abutments, were considered for the bridge replacement at this location. The selected bridge type for the purposes of this report is a single span precast prestressed AASHTO box beam bridge with full height abutments. As discussed in the Drainage section, the single span bridge was required to improve flow in the wash and mitigate effects of the proposed roadway improvements on the current floodplain elevation. The new bridge width and profile will be set to match the proposed roadway widening and adjusted roadway profile.

The proposed bridge geometry will consist of a 12 -foot wide westbound travel lane, a 16 -foot wide eastbound travel lane, a 12 -foot wide left turn lane, 6 -foot shoulders in each direction and $5^{\prime}-10^{\prime \prime}$ sidewalk with ADOT Combination Pedestrian Traffic Barrier Railing in each direction for an overall bridge width of $66-\mathrm{ft}$. The overall bridge length will be $70.5-\mathrm{ft}$. The bridge profile will be raised slightly from the existing bridge profile to match the proposed roadway improvements.

The bridge abutments will be full height abutments supported on drilled shafts. The existing wash banks on the inlet and outlet of the bridge will be protected with slope protection

### 5.0 Grade Separated Railroad Crossing

A detailed analysis for grade separated railroad crossings is not included in this report due to the economic infeasibility and construction impacts associated with this option. The minimum vertical clearance for a bridge over the UPRR is 23.5 feet per the BNSF-UPRR Guidelines for Railroad Grade Separated Projects. Adding the depth of structure would increase the roadway elevation approximately 30 feet above existing ground. Implementing the maximum allowable grade from the AASHTO Green Book and the ADOT Roadway Design Guidelines (RDG) would require ramps approximately 400 feet in length. Business and residential access fronting the face of the ramp retaining walls would be closed and require access from other locations along the site. Similar projects of this scope encountered construction costs in the $\$ 10$ million to $\$ 15$ million range not including design, right-of-way and utility costs.

### 6.0 Estimated Cost

### 6.1 Construction

An itemized construction cost estimate for each location is shown in Figures 6, 7, \& 8. Calle Sonora alternatives were not estimated separately because for planning purposes the "jug handle" alternative is comparable in cost to the roundabout. No funds have currently been allocated for the project.

### 6.2 Design

Design costs are broken out by project as follows: Gold Hill Road \$369,000; Produce Row \$217,000; Calle Sonora \$405,000.

Figure 6, Gold Hill Rd Conceptual Cost Estimate

| Federal No: N/A | Project Description: Gold Hill Road Cost Estimate |
| :--- | ---: |
| TRACS No: N/A | Project Location: Nogales, Arizona |
| Project No: N/A | Stage: Preliminary |
| Date: | July, 2015 |


| ITEM NO. | ITEM DESCRIPTION | UNIT | QUANTITY | UNIT PRICE |  | MOUNT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2010001 | Clearing and Grubbing | L.S. | 1 | \$ 10,000.00 | \$ | 10,000 |
| 2020001 | Removal of Structures \& Obstructions | L.S. | 1 | \$ 60,000.00 | \$ | 60,000 |
| 2030300 | Roadway Excavation | C.Y. | 3,815 | \$ 15.00 | \$ | 57,225 |
| 2030904 | Borrow | C.Y. | 7,230 | \$ 12.00 | \$ | 86,760 |
| 3030003 | Aggregate Base | C.Y. | 1,166 | \$ 60.00 | \$ | 69,960 |
| 4090003 | Asphaltic Concrete (Miscellaneous Structural) | Ton | 2,330 | \$ 90.00 | \$ | 209,700 |
| 5150002 | Utility Relocation Work | L.S. | 1 | \$ 40,000.00 | \$ | 40,000 |
| 6080107 | Miscellaneous Work (Signs) | L.S. | 1 | \$ 12,000.00 | \$ | 12,000 |
| 7040015 | Pavement Markings | L.S. | 1 | \$ 8,000.00 | \$ | 8,000 |
| 7330029 | Traffic Signal | L.S. | 1 | \$ 200,000.00 | \$ | 200,000 |
| 8080012 | Seeding and Miscellaneous Landscape Work | L.S. | 1 | \$ 15,000.00 | \$ | 15,000 |
| 9130100 | Concrete Channel Lining | S.Y. | 230 | \$ 120.00 | \$ | 27,600 |
| 9050001 | Guard Rail, W-Beam, Single Face | L.F. | 350 | \$ $\quad 15.00$ | \$ | 5,250 |
| 9050041 | Guard Rail End Terminal Assembly | EACH | 4 | \$ 2,500.00 | \$ | 10,000 |
| 9080050 | Concrete Curb and Gutter | L.F. | 2,344 | \$ 26.00 | \$ | 60,944 |
| 9080201 | Concrete Sidewalk | S.F. | 2,444 | \$ 6.00 | \$ | 14,664 |
| 9080288 | Curb Access Ramp | EACH | 4 | \$ 1,600.00 | \$ | 6,400 |
| 9080302 | Concrete Driveway | EACH | 2 | \$ 2,200.00 | \$ | 4,400 |
| 9300128 | Miscellaneous Work 18 (Drainage Improvements) | L.S. | 1 | \$ 20,000.00 | \$ | 20,000 |
| 9300201 | Railroad Personnel, Protective Crossings and Private Crossings | L.S. | 1 | \$ 150,000.00 | \$ | 150,000 |
|  | Bridge | L.S. | 1 | \$ 890,000.00 | \$ | 890,000 |
| ROADWAY AND BRIDGE SUBTOTAL |  |  |  |  | \$ | 1,957,903 |
|  |  |  |  |  |  |  |
|  | Construction Work Contingency | Percent | 20\% |  | \$ | 391,581 |
| SUBTOTAL |  |  |  |  | \$ | 2,349,484 |
|  |  |  |  |  |  |  |
|  | Construction Surveying and Layout | Percent | 3\% |  | \$ | 70,485 |
|  | Erosion Control | Percent | 2\% |  | \$ | 46,990 |
|  | Contractor Quality Control | Percent | 2\% |  | \$ | 46,990 |
|  | Furnish Water Supply | Percent | 2\% |  | \$ | 46,990 |
|  | Maintenance and Protection of Traffic | Percent | 10\% |  | \$ | 234,948 |
|  |  |  |  | SUBTOTAL | \$ | 2,795,887 |
|  |  |  |  |  |  |  |
|  | Mobilization | Percent | 10\% |  | \$ | 279,589 |
| CONSTRUCTION SUBTOTAL |  |  |  |  | \$ | 3,075,476 |
|  |  |  |  |  |  |  |
|  | Construction Administration | Percent | 10\% |  | \$ | 279,589 |
| CONSTRUCTION TOTAL COST |  |  |  |  | \$ | 3,355,065 |
|  |  |  |  |  |  |  |
|  | Design Costs | Percent | 12\% | Cst Subtotal | \$ | 369,057 |
|  | Right-of-Way |  |  |  | \$ | 179,400 |
| TOTAL PROJECT COST |  |  |  |  | \$ | 3,903,522 |

Figure 7, Produce Row Conceptual Cost Estimate

| Federal No: |  | Project Description : Produce Row Cost Estimate |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TRACS No: | N/A | Project Location : Nogales, Arizona |  |  |  |  |
| Project No : | N/A | Stage : Preliminary |  |  |  |  |
| Date: | July, 2015 | Project Manager : Scott Altherr, PE |  |  |  |  |
| ITEM NO. | ITEM DESCRIPTION | UNIT | QUANTITY | UNIT PRICE |  | MOUNT |
| 2010001 | Clearing and Grubbing | L.S. | 1 | \$ 10,000.00 | \$ | 10,000 |
| 2020001 | Removal of Structures \& Obstructions | L.S. | 1 | \$ 30,000.00 | \$ | 30,000 |
| 2050001 | Grading Roadway for Pavement | S.Y. | 1,890 | \$ 5.00 | \$ | 9,450 |
| 3030003 | Aggregate Base | C.Y. | 315 | \$ 60.00 | \$ | 18,900 |
| 4090003 | Asphaltic Concrete (Miscellaneous Structural) | Ton | 629 | \$ 90.00 | \$ | 56,610 |
| 5150002 | Utility Relocation Work | L.S. | 1 | \$ 20,000.00 | \$ | 20,000 |
| 6080107 | Miscellaneous Work (Signs) | L.S. | 1 | \$ 3,000.00 | \$ | 3,000 |
| 7040015 | Pavement Markings | L.S. | 1 | \$ 2,000.00 | \$ | 2,000 |
| 7330029 | Traffic Signal | L.S. | 1 | \$ 50,000.00 | \$ | 50,000 |
| 8080012 | Seeding and Miscellaneous Landscape Work | L.S. | 1 | \$ 5,000.00 | \$ | 5,000 |
| 9080050 | Concrete Curb and Gutter | L.F. | 182 | \$ 26.00 | \$ | 4,732 |
| 9080288 | Curb Access Ramp | EACH | 2 | \$ 1,600.00 | \$ | 3,200 |
| 9130100 | Concrete Channel Lining | S.Y. | 700 | \$ 120.00 | \$ | 84,000 |
| 9300128 | Miscellaneous Work 18 (Drainage Improvements) | L.S. | 1 | \$ 8,000.00 | \$ | 8,000 |
| 9300201 | Railroad Personnel, Protective Crossings and Private Crossings | L.S. | 1 | \$ 150,000.00 | \$ | 150,000 |
|  | Bridge | L.S. | 1 | \$ 750,000.00 | \$ | 750,000 |
| ROADWAY AND BRIDGE SUBTOTAL |  |  |  |  | \$ | 1,204,892 |
|  |  |  |  |  |  |  |
|  | Construction Work Contingency | Percent | 20\% |  | \$ | 240,978 |
| SUBTOTAL |  |  |  |  | \$ | 1,445,870 |
|  |  |  |  |  |  |  |
|  | Construction Surveying and Layout | Percent | 3\% |  | \$ | 43,376 |
|  | Erosion Control | Percent | 2\% |  | \$ | 28,917 |
|  | Contractor Quality Control | Percent | 2\% |  | \$ | 28,917 |
|  | Furnish Water Supply | Percent | 2\% |  | \$ | 28,917 |
|  | Maintenance and Protection of Traffic | Percent | 10\% |  | \$ | 144,587 |
| SUBTOTAL |  |  |  |  | \$ | 1,720,584 |
|  |  |  |  |  |  |  |
|  | Mobilization | Percent | 10\% |  | \$ | 172,058 |
| CONSTRUCTION SUBTOTAL |  |  |  |  | \$ | 1,892,642 |
|  |  |  |  |  |  |  |
|  | Construction Administration | Percent | 15\% |  | \$ | 258,088 |
| CONSTRUCTION TOTAL COST |  |  |  |  | \$ | 2,150,730 |
|  |  |  |  |  |  |  |
|  | Design Costs | Percent | 12\% | Cst Subtotal | \$ | 227,117 |
|  | Right-of-Way |  |  |  | \$ | 158,196 |
| TOTAL PROJECT COST |  |  |  |  | \$ | 2,536,043 |

Figure 8, Calle Sonora Conceptual Cost Estimate

| Federal No: |  | Project Description: Calle Sonora Cost Estimate |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TRACS No: | N/A | Project Location: Nogales, Arizona |  |  |  |  |
| Project No: | N/A | Stage : Preliminary |  |  |  |  |
| Date: | July, 2015 | Project Manager : Scott Altherr, PE |  |  |  |  |
| ITEM NO. | ITEM DESCRIPTION | UNIT | QUANTITY | UNIT PRICE |  | MOUNT |
| 2010001 | Clearing and Grubbing | L.S. | 1 | \$ 25,000.00 | \$ | 25,000 |
| 2020001 | Removal of Structures \& Obstructions | L.S. | 1 | \$ 50,000.00 | \$ | 50,000 |
| 2050001 | Grading Roadway for Pavement | S.Y. | 6,914 | \$ 5.00 | \$ | 34,570 |
| 3030003 | Aggregate Base | C.Y. | 1,155 | \$ 60.00 | \$ | 69,300 |
| 4090003 | Asphaltic Concrete (Miscellaneous Structural) | Ton | 2,305 | \$ 90.00 | \$ | 207,450 |
| 5150002 | Utility Relocation Work | L.S. | 1 | \$ 30,000.00 | \$ | 30,000 |
| 6080107 | Miscellaneous Work (Signs) | L.S. | 1 | \$ 9,000.00 | \$ | 9,000 |
| 7040015 | Pavement Markings | L.S. | 1 | \$ 6,000.00 | \$ | 6,000 |
| 7330029 | Traffic Signal | L.S. | 1 | \$ 100,000.00 | \$ | 100,000 |
| 8080012 | Seeding and Miscellaneous Landscape Work | L.S. | 1 | \$ 10,000.00 | \$ | 10,000 |
| 9080002 | Concrete Curb | L.F. | 603 | \$ 20.00 | \$ | 12,060 |
| 9080050 | Concrete Curb and Gutter | L.F. | 2,255 | \$ 26.00 | \$ | 58,630 |
| 9080150 | Concrete Median Pavement | S.F. | 2,036 | \$ 7.00 | \$ | 14,252 |
| 9080201 | Concrete Sidewalk | S.F. | 7,408 | \$ 6.00 | \$ | 44,448 |
| 9080288 | Curb Access Ramp | EACH | 8 | \$ 1,600.00 | \$ | 12,800 |
| 9080302 | Concrete Driveway | EACH | 2 | \$ 2,200.00 | \$ | 4,400 |
| 9130100 | Concrete Channel Lining | S.Y. | 400 | \$ 120.00 | \$ | 48,000 |
| 9300128 | Miscellaneous Work 18 (Drainage Improvements) | L.S. | 1 | \$ 15,000.00 | \$ | 15,000 |
| 9300201 | Railroad Personnel, Protective Crossings and Private Crossings | L.S. | 1 | \$ 200,000.00 | \$ | 200,000 |
|  | Bridge | L.S. | 1 | \$ 1,200,000.00 | \$ | 1,200,000 |
| ROADWAY AND BRIDGE SUBTOTAL |  |  |  |  | \$ | 2,150,910 |
|  |  |  |  |  |  |  |
|  | Construction Work Contingency | Percent | 20\% |  | \$ | 430,182 |
| SUBTOTAL |  |  |  |  | \$ | 2,581,092 |
|  |  |  |  |  |  |  |
|  | Construction Surveying and Layout | Percent | 3\% |  | \$ | 77,433 |
|  | Erosion Control | Percent | 2\% |  | \$ | 51,622 |
|  | Contractor Quality Control | Percent | 2\% |  | \$ | 51,622 |
|  | Furnish Water Supply | Percent | 2\% |  | \$ | 51,622 |
|  | Maintenance and Protection of Traffic | Percent | 10\% |  | \$ | 258,109 |
| SUBTOTAL |  |  |  |  | \$ | 3,071,500 |
|  |  |  |  |  |  |  |
|  | Mobilization | Percent | 10\% |  | \$ | 307,150 |
| CONSTRUCTION SUBTOTAL |  |  |  |  | \$ | 3,378,650 |
|  |  |  |  |  |  |  |
|  | Construction Administration | Percent | 10\% |  | \$ | 307,150 |
| CONSTRUCTION TOTAL COST |  |  |  |  | \$ | 3,685,800 |
|  |  |  |  |  |  |  |
|  | Design Costs | Percent | 12\% | Cst Subtotal | \$ | 405,438 |
|  | Right-of-Way |  |  |  | \$ | 696,582 |
| TOTAL PROJECT COST |  |  |  |  | \$ | 4,787,820 |

### 7.0 Project Action Item Checklist

- Submit constraints analysis to Public Works Department
- Submit constraints analysis for courtesy review to Flood Control District and ADOT
- Present findings at City Council meeting
- Begin right-of-way acquisition process
- Set aside and budget funding for design and construction
- Scope the final design and construction documents.
- Obtain Section 404 Clean Water Act Permit
- Prepare Plans, Specifications, and Estimate for first project.
- Begin utility relocation
- Advertise for Construction Bids
- Construct


### 8.0 Study Limitations

The intent of this analysis is to provide a scoping document that analyzes the constraints and possible solutions and provides a significant step forward in the planning process to budget and deliver projects for these crossings. Detailed design issues such as restoring access, construction phasing, and traffic control need further analysis. It is anticipated that with the congested nature of these project areas that any project development will have the interest of the general public, emergency services, business community, and utility industry as well as agencies such as ADOT, Santa Cruz County Flood Control District, and Union Pacific. Some assumptions that were made that could have an effect on cost of these projects are:

- No improvements outside of signalization, signing and striping will be required for connections to Grand Ave (B-19).
- Lighting of intersections will not impact overhead utilities and approaches to intersections do not require additional lighting.
- $20 \%$ Contingency is sufficient to cover unknown costs at this conceptual stage
- Geotechnical investigation will not discover any constraints that will increase the cost of construction
- De-watering of channel during construction is a given and is buried into bridge costs.


### 9.0 Preliminary Plans

The Preliminary Plans show the conceptual horizontal alignments, roadway improvements and proposed bridge structures for Gold Hill Road, Produce Row and Calle Sonora. These plans were prepared without design level survey, survey control, photometric analysis and geotechnical design recommendations. When these projects are advanced to final design each of these components will be added and the resulting information may require some modification of the conceptual plans and cost. The Preliminary Plans are shown in Appendix A.

## Appendix A

## Preliminary Plans










GENERAL NOTES:
Construction Specification
arizona Department of Transportation Standard Specifications
for Road and Bridge Construction, Edition of 2008 .
Design Specifications -
AASHTO LRFD Bridge Design Specifications, 6th Edition, 2012. Dead Load - Dead Load includes an allowance of 25 pounds per
square foot for future wear ing surface. Loading Class HL-93.
All concrete shall be Class 'S' unless noted otherwise.
Reinforcing steel shall conform to ASTM Specification A615. All
reinforcing shall be furnished as Grade 60.
All bends and hooks shall meet the requirements of AASHTO Articie 5. 10. 2 All bend dimensions for reinforcing steel shall
be out-to-oot of bars. Al placement dimensions for reinforcing
steel shal be to be out-toout of bars. Al phacement dimensions for rein
steel shall be to center of bars unless noted otherwise.
All reinforcing steel shall have 2 inch clear cover unless noted
Barriers shall be constructed after spans have taken dead load
deflection. Barriers shall not be slip formed. Dimensions shall not be scaled from drawings. Chamfer all exposed corners $3 / 4 "$ per Chamfer Detail unless
noted otherwise.

2. Elevations are measured along profile


OPTION 1 - PROPOSED SECTION
Scale: $1 / 4 "=1$ '0"


OPTION 2 - PROPOSED SECTION
Scale: $1 / 4 \mathrm{n}=1 \mathrm{l}-0 \mathrm{C}$


1. Stationing and dimensions measured along
E Calle Sonora Centerline.
2. Elevations are measured along profile
grade line. grade line


GENERAL NOTES:
Construction Specification

## Specifications for Road and Bridge Construction, Edition of 2008.

- 

Design Specifications -
AASHTO LRFD Bridge Design Specifications 6th Edition 2012
 for future wearing surface.
Loading Class - HS2O-44 and/or Interstate Alternate Loading. Composite Design-
mposite Design -ied by box beams only. Box beams are
Dead Ioad carrict
designed using transformed section properties.
All concrete shall be Class "S" unless noted otherwise.
Reinforcing steel shall conform
All
reinforcing shall be furnished as Specification
Grade 60 .
All bends and hooks shall meet the requirements of AASHTO Article 5.10 .2 All bend dimensions for reinforcing steel
shall be out-to-out of bars. All placement dimensions for Shall be out-to-out of bars. All placement dimensions for
reinforcing steel shall be to center of bars unless noted
therwise. retnforcinn
otherwise.
All reinforcing steel shall have 2 inch clear cover unless
noted otherwise.
Barrier shall be constructed after spans have taken dead
Ioad deflection. Barrier shall| not be silp formed.
Dimensions shall not be scaled from the drawings.
Chamer all exposed corners $3 / 4 "$ per Chamfer Detail unless
noted otherwise.


## Appendix B

## Traffic Evaluation

# Nogales Constraints Analysis Traffic Evaluation 

June 19, 2015

Prepared for:
City of Nogales

Prepared by:
Kimley»)Horn

333 E. Wetmore Road, Suite 280<br>Tucson, Arizona 85705

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## 1. INTRODUCTION

## Background Information

The City of Nogales is conducting a study that will determine potential improvements for three side streets east of Grand Avenue with potential replacement of three bridges that span across the Nogales Wash. The side streets include: Gold Hill Road, Produce Row, and Calle Sonora. The overall study will encompass a set of analysis to determine feasibility and conceptual cost of improving access, capacity, alignment geometry, and accommodating overweight vehicles and projected traffic volumes. This document provides the results of the traffic analysis portion of the study.

## Objectives of the Study

This section of the evaluation will document the analysis of current and future traffic conditions. The objectives of the traffic study include the following:

- Determine existing traffic conditions based on collected peak-hour turning movement counts, 24 -hour tube counts with truck classification data, 3-year crash history within the study limits. Also, a set of interviews with warehouse operators/stakeholders to understand their perspectives on existing conditions and transport needs were conducted.
- Forecast future traffic conditions at each of the 3 locations based on anticipated growth and development plans based on the stakeholder interview process.
- Perform a traffic analysis on current and future traffic.


## 2. EXISTING CONDITIONS

The study area encompasses 3 streets along Grand Avenue that provide access to a number of warehouses in the area. The streets include Gold Hill Road, Produce Row, and Calle Sonora. Each street has a bridge that crosses over the Nogales Wash. Figure 2 illustrates current lane configuration.

## Grand Avenue

Grand Avenue, also known as the Tucson-Nogales Highway is a major North/South arterial that connects to the Mexico border south of the city and connects to I-19 north of the city. Grand Avenue consists of segments with a 4-lane cross-section. Segments consist of having a center Two-Way-Left-Turn (TWLT) lane and other segments have a 4-lane median separated crosssections. The posted speed limit on Grand Avenue is 40 MPH. According to data provided by the South Eastern Arizona Governments Organization (SEAGO), Grand Avenue has an Annual Average Daily Traffic (AADT) of 17,600 vehicles (2013).

## Gold Hill Road

Gold Hill Road is a 2-lane collector street located north within the project limits. The street intersects with Grand Avenue which then becomes Mesa Verde Road, west of Grand Avenue. The intersection is signalized. Based on the 24 -hour traffic data collected, Gold Hill Road has approximately 3,000 vehicle per day (VPD). The road gives access to multiple warehouses and residential areas further east. The road is estimated to have a 25 MPH speed limit. The intersection of Grand Avenue and Gold Hill Road is signalized. According to a site visit, the cycle length of the signal was estimated to be 80 seconds with Permissive left turns for each approach.

## Produce Row

Produce Row is a 2-lane collector street centrally located within the project limits with a speed limit of 25 MPH. The street intersects with Grand Avenue which then becomes Frank Reed Road, west of Grand Avenue. The intersection is signalized. Based on the 24 -hour traffic data collected, Produce Row has approximately 2,000 VPD. The road provides access primarily to Warehouses with no residential access. According to a site visit, the cycle length of the signal was estimated to be 80 seconds in length with permissive/protected lefts for the northbound and southbound direction.

## Calle Sonora

Calle Sonora is a 2-lane collector street located south within of the project limits with a speed limit of 25 MPH. The street intersects with Grand Avenue which then becomes Mariposa Road, west of Grand Avenue The intersection is signalized. Based on the 24 -hour traffic data
collected, Calle Sonora has approximately 4,500 VPD. The road provides access to some warehouses and residential areas within Santa Cruz County. According to a site visit the cycle length was estimated to be 130 seconds long with split phasing for the east/west bound direction.

## Union Pacific Railroad

The Union Pacific Railroad (UPRR) runs at-grade through each of the 3 cross-streets, parallel to Grand Avenue just to the east. According to comments from Fresh Produce Association of America (FPAA) members, approximately 5-7 trains pass through on a daily basis at low speeds resulting in approximately 10-20 minute periods where the side-streets are inaccessible.

## Stakeholder Interviews

Stakeholder interviews with members of the Fresh Produce Association of the Americas (FPAA) were conducted on March $6^{\text {th }}$, 2015. The FPAA is an influential group that works to ensure uninterrupted access to Mexican grown fruits and vegetables. The objective of the interviews were to gain a local perspective of existing conditions but also determine what the future needs in terms of traffic growth are anticipated. Discussion points from the interviews are presented in various sections of the traffic report when appropriate. A summary of the stakeholder comments can be found in Appendix B.

Figure 1 - Existing Lane Configuration


## Traffic Data Collection

Traffic data was collected on February $4^{\text {th }}$, 2015. The traffic data was collected during what would be considered the peak season for produce shipments from Mexico. The collected traffic data includes 24 -hour tube counts located on the 3 bridges and AM/PM peak period intersection turning movement counts. Figure $\mathbf{2}$ illustrates the 24 -hour traffic volumes pattern.

Figure 2 - 24-hour Traffic Volume Profile


Figure $\mathbf{3}$ illustrates AM/PM peak-hour turning movement volumes at each of the study intersections.

Figure 3 - Existing Traffic Volumes


## Truck Volumes

A vehicle classification study was performed during the time when the 24-hour tube counts were collected. Vehicles were classified using the Federal Highway Association's (FHWA) 13Category vehicle classification scheme. The categories depend on whether the vehicle carries passengers or commodities. Non-passenger vehicles are further subdivided by number of axles and number of units, including both power and trailer units. Figure 4 illustrates the FHWA 13Category vehicle classification scheme.

Figure 4 - FHWA Vehicle Classifications


As shown in Figure 5, each of the three side streets shows a unique distribution of vehicle types throughout the day. A majority of the truck traffic include Single Unit 2-Axle trucks, Single Unit 3-Axle trucks and Single Trailer 5-Axle trucks. Also, Multi-Trailer 7 or More-Axle trucks may be encountered on Gold-Hill Road and Produce Row. According to the traffic data collected, each side street consists of the following truck percentages:

- Gold-Hill Road: 19\% Trucks
- Produce Row: 30\% Trucks
- Calle Sonora: 5\% Trucks

Figure 5 - Existing Vehicle Class Frequency


## Crash Analysis

Historic crash data was only available within the vicinity of the Grand Avenue and Gold Hill Road intersection. The crash data ranged from 2006-2015 with a total of 10 crashes reported by the Nogales Police Department. The crash statistics available included:

- Severity: 6 of the crashes resulted in injuries, 1 fatality, 1 damaged property, 2 other crashes reported as Hit/Run.
- None of the crashes were reported as alcohol related
- 6 of the reported crashes involved trucks with 1 of the truck involved crashes resulting in a fatality.
- 4 of the reported crashes were results of a vehicle's failure to yield, though one crash was argued that a truck in the southbound turning lane obstructed the view of conflicting traffic.
- 2 of the reported crashes were results of vehicles running a red light.

Other crash statistics for Calle Sonora \& Hohokam Drive (data from the Road Safety Assessment Mariposa Road /Target Range Road Calle Sonora/Hohokam Drive performed in 2009) include:

- Severity: 3 non-incapacitating/possible injury, 14 property damage only
- 7 rear-end (includes 2 backing crashes)
- 6 right angle
- 2 sideswipe same direction
- Traffic queues on westbound Calle Sonora due to Grand Avenue signal and train cited in 4 crashes
- Tractor trailers involved in 6 crashes


## Existing Traffic Analysis

A capacity analysis of existing transportation facilities and traffic volumes was conducted for this study.

## Analysis Methodology

Capacity analysis is an iterative process that demonstrates the relationship between traffic operations and roadway/intersection geometry, assesses deficiencies, and identifies alternatives. Capacity analysis is performed based on methodologies outlined in the Highway Capacity Manual (Transportation Research Board, 2000). The Highway Capacity Manual (HCM) employs methodologies to calculate intersection LOS. LOS is a qualitative assessment of the quantitative effect of factors such as intersection geometry, lane configuration, and traffic volumes. Operating conditions are categorized as " $A$ " through " $F$," with " $A$ " representing the most favorable conditions and "F" representing the least favorable. LOS "D" for signalized intersections is equal to being delayed at the intersection for less than 35-55 seconds per vehicle. Table 1 shows the delay (wait time thresholds) for each LOS grade.

Table 1 - Level of Service Delay Thresholds

| LOS | Signalized Intersection | Unsignalized Intersection |
| :--- | :--- | :--- |
| A | $\leq 10 \mathrm{sec}$ | $\leq 10 \mathrm{sec}$ |
| B | $10-20 \mathrm{sec}$ | $10-15 \mathrm{sec}$ |
| C | $20-35 \mathrm{sec}$ | $15-25 \mathrm{sec}$ |
| D | $35-55 \mathrm{sec}$ | $25-35 \mathrm{sec}$ |
| E | $55-80 \mathrm{sec}$ | $35-50 \mathrm{sec}$ |
| F | $\geq 80 \mathrm{sec}$ | $\geq 50 \mathrm{sec}$ |

Intersection LOS is computed as a weighted average of vehicle delay. An intersection may have an acceptable overall LOS but may also have individual movements with unacceptable LOS. As a result, all movements are analyzed individually, and recommendations are made to reduce delay and increase capacity on critical movements.

Synchro was used to determine the LOS for each movement at each intersection. This enabled the identification of improvements that would needed at each intersection to maintain a LOS of "D" or better, consistent with most urban areas' engineering policy.

As shown in Table 2, the capacity analysis shows the traffic operational performance for each intersection and individual movements. Grand Avenue \& Calle Sonora has the worst performance of the three intersections which is due to the higher volumes that currently exist at the intersection. However, LOS D is typically considered acceptable within urban areas.

It is important to note that the capacity analysis may not capture actual traffic conditions. Such an analysis would require a micro-simulation analysis with an extensive calibration procedure. Thus, the capacity analysis may show that the intersection is performing better than what is actually experienced. However, field observations and feedback from FPAA members described that roadway geometry constraints, especially for trucks maneuvering through the intersections are the governing factors for the traffic conditions.

Table 2 - Existing Intersection Level-of-Service

| Local Intersections | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Intersection LOS | Traffic Control |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |  |
| Grand Avenue \& Gold Hill Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Hour | B |  |  | B |  |  | A | B |  | B | A |  | B | Signalized |
| PM Peak Hour | B |  |  | A |  |  | B |  |  | B |  |  | B |  |
| Grand Avenue \& Produce Row |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Hour | D | A |  |  | A |  | A | B |  | A | C |  | C | Signalized |
| PM Peak Hour | C | A |  |  | B |  | B | C |  | B | C |  | B |  |
| Grand Avenue \& Calle Sonora |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Hour | D | D | B |  | D |  | D |  |  | E | D | B | D | Signalized |
| PM Peak Hour | E | D | A |  | E |  | E |  |  | E | D | B | D |  |
| Calle Sonora \& Hohokam Road |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| AM Peak Hour |  | A |  |  | A |  |  | B |  |  | B |  | A | Unsignalized |
| PM Peak Hour |  | A |  |  | A |  |  | C |  |  | B |  | A |  |

## 3. FUTURE TRAFFIC CONDITIONS

As documented from the stake-holder interviews prior to this study, truck traffic is inevitably going to increase within the study areas as the operations of the warehouses and distribution facilities expand or as new ones get constructed. From the stakeholder interviews, it was mentioned that the Nogales Port of Entry (POE) currently has approximately 1800 trucks pass through the POE per day from Mexico during the peak season and this is expected to double in approximately 10 years. With recent improvements to the Mariposa Port of Entry, the facility may have the capacity to process up to 4,000 trucks daily. FPAA members mentioned that various warehouses are unique and each facility anticipates different Mexican to American truck ratios. Though, the standard rule-of-thumb seems to be that for every truck that comes into Nogales from Mexico, 2 American trucks come into Nogales. Also, peak seasons vary among the facilities though, typically the peak season is considered to be from February - May. According to an FPAA presentation, fresh produce crossing from Mexico showed an increase of $17 \%$ in 2012-2013 in Nogales. However, it was discussed that an average growth of 6-8 percent per year is typical, on average.

## Traffic Forecast

A traffic forecast was performed at each study intersection and roadway segment. The forecast was based on multiple sources of references including the information gathered from the stakeholder interviews, mainly FPAA members, and the 2010 Unified Nogales Santa Cruz County Transportation Plan. The objective of the forecast is to observe the future needs of the intersection and future cross-section requirements of the three bridges.

Listed are assumptions that were considered for the traffic forecast:

- For consistency with the 2010 transportation plan, traffic volumes were forecasted for 2030. Inbound daily truck traffic from Mexico coming into the POE is expected to double by this time.
- According to the Unified Nogales Santa Cruz County Transportation Plan 2010, Grand Avenue is expected to see $30 \%$ traffic growth in 2030. The major factors influencing the forecast include future housing and employment, Port of Entry to and from Mexico, and magnitude of traffic to and from Pima County and points beyond.
- The growth rates that were used from the Unified Nogales Santa Cruz County Transportation Plan 2010 traffic estimation assumed that both car and truck traffic were included in the rate. In this case, existing truck percentages were maintained.
- Produce Row, east of Grand Avenue shows no opportunity for residential growth but has potential for Warehouse expansion and increased truck traffic. A growth rate for trucks was applied.

A summary of the 2030 traffic forecast is shown in Table 3.

Table 3-2030 Traffic Forecast

| Road | Growth Rate | Description |
| :---: | :---: | :---: |
| Grand Avenue | 30\% | Corridor wide growth rate on Grand Avenue, as forecasted in the Unified Nogales Santa Cruz County Transportation Plan 2010 |
| WB Gold Hill Road (East of Grand Avenue) | 14\% | Interpolated using the 2010 Unified Nogales Santa Cruz County Transportation Plan estimated \& forecasted housing Units from 2015 to 2030. |
| Gold Hill Road, Produce Row, Calle Sonora (Trucks Only) | 6\% | Based on the average estimated truck loads from Mexico, Southwest Border Crossing Trends (FPAA). |
| EB Frank Reed Road (West of Grand Avenue at Produce Row) | 30\% | Growth rate based on the 2010 Unified Nogales Santa Cruz County Transportation Plan for Frank Reed Road, east of Grand Avenue. |
| Calle Sonora/Mariposa Road | 30\% | Growth rate based on the 2010 Unified Nogales Santa Cruz County Transportation Plan. |
| Hohokam Drive/Smokey Lane (Trucks Only) | 6\% | Based on the average estimated truck loads from Mexico, Southwest Border Crossing Trends (FPAA). |

Figure 6 illustrates the future traffic volumes for both AM/PM peak periods.

Figure 6 - Estimated Future Peak-Hour Traffic Volumes


## Future Year Traffic Analysis

An analysis was performed using the estimated future peak-hour volumes, as illustrated in Figure 6. The potential geometric enhancements for the intersections and bridges, to accommodate heavy-truck volumes, were incorporated into the analysis and additional enhancements were identified based on a future-year capacity analysis. In addition to the capacity analysis, access management, sight distance, and turn-lane warrants along Grand Avenue were used to identify the needs for safe and efficient circulation within the study intersections.

Table 4 illustrates the results of the capacity analysis based on the estimated future year traffic conditions. With the enhancements incorporated, intersection operations are expected to be maintained with increased future traffic volumes.

Table 4 - Estimated Future LOS

| Local Intersections | EB |  |  | WB |  |  | NB |  |  | SB |  |  | Intersection LOS | Traffic Control |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | L | T | R | L | T | R | L | T | R | L | T | R |  |  |

Grand Avenue \& Gold Hill Road

|  |  |  |  |  |  |  |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AM Peak Hour | C | A | C | A | D | B | D | D | C | Signalized |
| PM Peak Hour | C | A | C | B | D | C | D | C | C |  |

Grand Avenue \& Produce Row

| AM Peak Hour | E | A | A | C | A | B | A | D | C | Signalized |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PM Peak Hour | C | A | C | A | A | C | A | B | B |  |

Grand Avenue \& Calle Sonora

| AM Peak Hour | C | C | A | C | D | A | E | C | D | C | A | C | Signalized |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PM Peak Hour | C | C | A | A | D | B | D | C | E | D | A | C |  |

## Calle Sonora \& Hohokam Road

| AM Peak Hour | A | A | B | B | A |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| PM Peak Hour | A | A | C | B | A | Unsignalized |

## 4. SUMMARY OF RECOMMENDATIONS

## Roadway-Bridge Cross-section

Both safety and traffic operational concerns due to the continuous heave truck traffic require the need for a wider cross-section at the three locations. According to field observations and feedback from FPAA members, trucks turning from cross-streets must overtake opposing lanes. Thus, interrupting opposing traffic which causes vehicles to queue up will increase unsafe situations that may lead to collisions.

To accommodate the heavy trucks turning from access drives or intersecting roadways, it is recommended to increase the roadway cross-section. The increased cross-section shall allow heavy trucks to execute turning maneuvers without utilizing the opposing lane. It is recommended that each of the three roadways consist of wider through lanes. Also, include a left-turn lane on the westbound approaches such that the storage length is extended east of the bridges as engineering constraints permit.

## Turn Lane Warrant

Turn Lane Warrants from the ADOT Traffic Engineering Policies, Guidelines, and Procedures (December 2014), Section 200, were utilized to determine the need for right-turn lanes on the northbound approaches of each of the three intersections along Grand Avenue. Existing and future traffic volumes justify the need for right-turn lanes at the 3 northbound approaches. However, due to the observed engineering constraints, such as right-of-way, utilities and bridge constraints, constructing right-turn lanes along Grand Avenue lanes would not be feasible.

## Intersection Operations

To improve intersection operations and accommodate the estimated future traffic volumes, it is recommended to implement the following concurrently with the construction of the new bridges

## Calle Sonora

- Construct an exclusive right-turn lane on the westbound approach of Calle Sonora, designed such that it meets ADOT minimum standards.
- With the exclusive westbound left-turn lane, reconfigure the traffic control signal for optimized standard phasing. Thus, removing the existing split-phasing as it would not be necessary with the enhanced intersection configuration would allow for efficient shorter cycle lengths.


## Produce Row

- Reconfigure the traffic control signal's cycle length to allow for turning trucks to completely clear the intersection during approaches green phase. Comments from the stakeholder interviews and observations shows that existing timing of the signal phases,
yellow change and red clearance intervals, especially right/left turning trucks, doesn't allow trucks to safely clear out of the intersection. Note that there is no standard practice or methods recommended for intersections with significant heavy truck percentages.


## Gold Hill Road

- It is recommended to construct an exclusive left-turn lane at the eastbound approach of Mesa Verde Road, designed such that it meets ADOT minimum standards. With the leftturn lane on the westbound approach as part of the Gold Hill Road enhancement, construction of the eastbound dedicated left-turn lane would not require split-phasing. Thus, reduce delays of the left/right turning vehicles during the peak periods.


## Access Management

The potential reconstruction of the 3 bridges and roadways, would allow for an opportunity to implement access management practices on each roadway. Access management allows for maintaining roadway safety and mobility by controlling access location, design, spacing and operation. The following is recommended to be implemented during the construction of the new bridges:

- At Calle Sonora, it is recommended to close 1 of the northbound access drive (Alex's Tires, Inc.) and relocate the southbound and northbound driveways, located west of the bridge. Relocate the access drives from the intersection of Grand Avenue / Calle Sonora to allow 150 ' minimum spacing between the access drives and the Grand Avenue curb line. A 150' minimum is typically a standard policy in many jurisdictions.
- Also, access drive turning restriction should be considered at the relocated driveways along Calle Sonora for both the north and south access drives due to the proximity to the signalized intersection. Allowing all movements may increase accident potential. Thus, consider a roadway cross-section that would restrict left-in and left-out movements on both driveways.
- At Produce Row, construct an access drive for the two businesses on the north and south of Produce Row, west of the bridge. Locate the dedicated access drives such that at a minimum 150 ' spacing or more exists between the access drive and the Grand Avenue curb line.
- With the construction of the eastbound exclusive left-turn lane on Mesa Verde Road, construct new access drives for both the north and south properties. Construct such that a minimum 150' spacing or more exists between the access drive and the Grand Avenue curb line.


## Appendix A - Traffic Count Data

## Project \#: 15-1041-001-Cars

## TMC SUMMARY OF Grand Ave, \& Gold Hill Rd.



Intersection Turning Movement
Prepared by:

## $\xrightarrow{\stackrel{\rightharpoonup}{\mid}} \stackrel{\text { Dield Data Services of Arizona, Inc. }}{520.316 .6745}$ <br> Veracitytrafficgroup

N-S STREET: Grand Ave.
DATE: 02/04/15
LOCATION: Nogales
E-W STREET: Gold Hill Rd.
DAY: WEDNESDAY
PROJECT\# 15-1041-001 - Cars

|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LANES: | $\begin{gathered} \mathrm{NL} \\ 1 \end{gathered}$ | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | NR 0 | $\mathrm{SL}$ | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | $\begin{gathered} \text { SR } \\ 0 \end{gathered}$ | $\begin{gathered} \mathrm{EL} \\ 0 \end{gathered}$ | $\begin{gathered} \mathrm{ET} \\ 1 \end{gathered}$ | $\begin{gathered} \text { ER } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WL } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WT } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 6:00 AM | CARS ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00 AM | 7 | 176 | 5 | 5 | 197 | 9 | 12 | 1 | 9 | 6 | 0 | 15 | 442 |
| 7:15 AM | 6 | 173 | 2 | 4 | 217 | 10 | 23 | 0 | 15 | 9 | 0 | 16 | 475 |
| 7:30 AM | 8 | 106 | 7 | 10 | 329 | 21 | 8 | 0 | 25 | 7 | 0 | 5 | 526 |
| 7:45 AM | 4 | 115 | 15 | 7 | 228 | 10 | 8 | 0 | 21 | 7 | 0 | 3 | 418 |
| 8:00 AM | 6 | 87 | 12 | 11 | 173 | 12 | 11 | 0 | 11 | 8 | 2 | 2 | 335 |
| 8:15 AM | 8 | 75 | 9 | 9 | 124 | 13 | 11 | 1 | 10 | 3 | 0 | 6 | 269 |
| 8:30 AM | 9 | 77 | 11 | 12 | 138 | 6 | 10 | 2 | 16 | 9 | 0 | 7 | 297 |
| 8:45 AM | 10 | 88 | 9 | 10 | 170 | 13 | 15 | 2 | 11 | 16 | 0 | 7 | 351 |
| 9:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 58 | 897 | 70 | 68 | 1576 | 94 | 98 | 6 | 118 | 65 | 2 | 61 | 3113 |
| Approach \% | 5.66 | 87.51 | 6.83 | 3.91 | 90.68 | 5.41 | 44.14 | 2.70 | 53.15 | 50.78 | 1.56 | 47.66 |  |
| App/Depart | 1025 | 1 | 1056 | 1738 | 1 | 1759 | 222 | 1 | 144 | 128 | 1 | 154 |  |

AM Peak Hr Begins at: 700 AM
PEAK

| Volumes | 25 | 570 | 29 | 26 | 971 | 50 | 51 | 1 | 70 | 29 | 0 | 39 | 1861 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Approach \% | 4.01 | 91.35 | 4.65 | 2.48 | 92.74 | 4.78 | 41.80 | 0.82 | 57.38 | 42.65 | 0.00 | 57.35 |  |

PEAK HR.
FACTOR:
0.830
0.727 |
$0.803 \quad \mid \quad 0.680$
0.885

CONTROL: Signal
COMMENT 1:
GPS:
31.383543, -110.947529

## Intersection Turning Movement

Field Data Services of Arizona, Inc.<br>520.316.6745

| N-S STREET: | Grand Ave. | DATE: 02/04/15 | LOCATION: Nogales |
| :--- | :--- | :---: | :--- |
| E-W STREET: | Gold Hill Rd. | DAY: WEDNESDAY | PROJECT\# |
| 15-1041-001-Cars |  |  |  |


|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LANES: | $\begin{gathered} \mathrm{NL} \\ 1 \end{gathered}$ | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | NR 0 | SL 1 | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | $\begin{gathered} \text { SR } \\ 0 \end{gathered}$ | $\begin{gathered} \mathrm{EL} \\ 0 \end{gathered}$ | ET 1 | ER 0 | $\begin{gathered} \text { WL } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WT } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 1:00 PM | CARS ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 20 | 177 | 7 | 10 | 183 | 14 | 17 | 1 | 15 | 13 | 1 | 7 | 465 |
| 4:15 PM | 26 | 157 | 6 | 9 | 130 | 8 | 21 | 2 | 13 | 13 | 1 | 14 | 400 |
| 4:30 PM | 19 | 167 | 14 | 7 | 150 | 5 | 18 | 2 | 19 | 12 | 4 | 8 | 425 |
| 4:45 PM | 21 | 172 | 15 | 14 | 158 | 11 | 11 | 0 | 9 | 10 | 0 | 8 | 429 |
| 5:00 PM | 11 | 196 | 11 | 6 | 147 | 16 | 22 | 2 | 15 | 15 | 2 | 15 | 458 |
| 5:15 PM | 16 | 189 | 10 | 7 | 144 | 14 | 13 | 3 | 15 | 15 | 1 | 12 | 439 |
| 5:30 PM | 15 | 193 | 13 | 11 | 151 | 10 | 18 | 1 | 12 | 16 | 2 | 13 | 455 |
| 5:45 PM | 14 | 175 | 11 | 11 | 145 | 18 | 23 | 1 | 14 | 13 | 3 | 15 | 443 |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 142 | 1426 | 87 | 75 | 1208 | 96 | 143 | 12 | 112 | 107 | 14 | 92 | 3514 |
| Approach \% | 8.58 | 86.16 | 5.26 | 5.44 | 87.60 | 6.96 | 53.56 | 4.49 | 41.95 | 50.23 | 6.57 | 43.19 |  |
|  |  | 1655 | 1 | 1661 | 1379 | $/$ | 1427 | 267 | 1 | 174 | 213 | 1 | 252 |
| App/Depart |  |  |  |  |  |  |  |  |  |  |  |  |  |

PM Peak Hr Begins at: 500 PM
PEAK

| Volumes | 56 | 753 | 45 | 35 | 587 | 58 | 76 | 7 | 56 | 59 | 8 | 55 | 1795 |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Approach \% | 6.56 | 88.17 | 5.27 | 5.15 | 86.32 | 8.53 | 54.68 | 5.04 | 40.29 | 48.36 | 6.56 | 45.08 |  |

PEAK HR.

CONTROL: Signal
COMMENT 1: 0
GPS:
31.383543, -110.947529

## Project \#: $\underline{\text { 15-1041-001-H.V. }}$

## TMC SUMMARY OF Grand Ave, \& Gold Hill Rd.



Intersection Turning Movement Prepared by:

##  <br> veracitytrafficgroup

N-S STREET: Grand Ave. DATE: 02/04/15 LOCATION: Nogales
E-W STREET: Gold Hill Rd. DAY: WEDNESDAY PROJECT\# 15-1041-001-H.V.

|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LANES: | NL 1 | NT 2 | NR 0 | SL 1 | ST 2 | $\begin{gathered} \text { SR } \\ 0 \end{gathered}$ | $\begin{gathered} \text { EL } \\ 0 \end{gathered}$ | ET 1 | ER 0 | WL 0 | $\begin{gathered} \text { WT } \\ \hline \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 6:00 AM | HEAVY VEHICLES ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00 AM | 0 | 4 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 7 |
| 7:15 AM | 0 | 3 | 0 | 1 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 2 | 9 |
| 7:30 AM | 0 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 6 |
| 7:45 AM | 0 | 3 | 0 | 3 | 7 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 14 |
| 8:00 AM | 0 | 5 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 8:15 AM | 0 | 4 | 0 | 1 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 8:30 AM | 0 | 8 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 11 |
| 8:45 AM | 0 | 5 | 1 | 0 | 4 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 12 |
| 9:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| VolumesApproach \%App/Depart | 0 | 33 | 1 | 6 | 27 | 2 | 0 | 0 | 1 | 2 | 0 | 7 | 79 |
|  | 0.00 | 97.06 | 2.94 | 17.14 | 77.14 | 5.71 | 0.00 | 0.00 | 100.00 | 22.22 | 0.00 | 77.78 |  |
|  | 34 | 1 | 40 | 35 | 1 | 30 | 1 | 1 | 7 | 9 | 1 | 2 |  |

AM Peak Hr Begins at: 745 AM
PEAK

| Volumes | 0 | 20 | 0 | 5 | 17 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 45 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach \% | 0.00 | 100.00 | 0.00 | 22.73 | 77.27 | 0.00 | 0.00 | 0.00 | 100.00 | 0.00 | 0.00 | 100.00 |  |

PEAK HR.
FACTOR:
0.625
$0.550 \quad \mid \quad 0.250$
0.250

CONTROL: Signal
COMMENT 1:
GPS:
31.383543, -110.947529

## Intersection Turning Movement

## $\xrightarrow{\text { Field Data Services of Arizona, Inc. }}$ <br> 520.316.6745 <br> veracitytrafficgroup

| N-S STREET: | Grand Ave. | DATE: 02/04/15 | LOCATION: Nogales |
| :--- | :--- | :--- | :--- |
| E-W STREET: | Gold Hill Rd. | DAY: WEDNESDAY | PROJECT\# |
| 15-1041-001-H.V. |  |  |  |


| LANES: | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \mathrm{NL} \\ 1 \end{gathered}$ | NT 2 | NR 0 | SL 1 | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | $\begin{gathered} \text { SR } \\ 0 \end{gathered}$ | $\begin{gathered} \mathrm{EL} \\ 0 \end{gathered}$ | $\begin{gathered} \text { ET } \\ 1 \end{gathered}$ | $\begin{gathered} \text { ER } \\ 0 \end{gathered}$ |  | $\begin{gathered} \text { WT } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 1:00 PM | HEAVY VEHICLES ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 0 | 12 | 5 | 3 | 13 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 35 |
| 4:15 PM | 0 | 6 | 5 | 2 | 10 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 26 |
| 4:30 PM | 0 | 10 | 2 | 3 | 10 | 0 | 0 | 0 | 0 | 3 | 0 | 1 | 29 |
| 4:45 PM | 0 | 8 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 17 |
| 5:00 PM | 0 | 7 | 2 | 2 | 12 | 0 | 0 | 0 | 0 | 3 | 0 | 3 | 29 |
| 5:15 PM | 0 | 14 | 0 | 2 | 14 | 0 | 0 | 0 | 0 | 3 | 0 | 2 | 35 |
| 5:30 PM | 0 | 10 | 3 | 2 | 6 | 0 | 0 | 0 | 0 | 4 | 0 | 1 | 26 |
| 5:45 PM | 0 | 17 | 2 | 1 | 9 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 32 |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 0 | 84 | 19 | 15 | 80 | 0 | 0 | 0 | 0 | 20 | 0 | 11 | 229 |
| Approach \% | 0.00 | 81.55 | 18.45 | 15.79 | 84.21 | 0.00 | \#\#\#\# | \#\#\#\# | \#\#\#\# | 64.52 | 0.00 | 35.48 |  |
| App/Depart | 103 | 1 | 95 | 95 | 1 | 100 | 0 | I | 34 | 31 | 1 | 0 |  |

PM Peak Hr Begins at: 500 PM
PEAK

| Volumes | 0 | 48 | 7 | 7 | 41 | 0 | 0 | 0 | 0 | 11 | 0 | 8 | 122 |
| :--- | :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :--- |


PEAK HR.
FACTOR:
| 0.724
0.750


| 0.000 |
| :-- |

0.792
0.871

CONTROL: Signal
COMMENT 1: 0
GPS:
31.383543, -110.947529

## Project \#: 15-1041-002-Cars

## TMC SUMMARY OF Grand Ave, \& Produce Row



Intersection Turning Movement
Prepared by:

## $\xrightarrow{\stackrel{\rightharpoonup}{\mid}} \stackrel{\text { Dield Data Services of Arizona, Inc. }}{520.316 .6745}$ <br> Veracitytrafficgroup

N-S STREET: Grand Ave.
DATE: 02/04/15
LOCATION: Nogales
E-W STREET: Produce Row
DAY: WEDNESDAY
PROJECT\# 15-1041-002 - Cars

|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LANES: | NL 1 | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | NR 0 | SL 1 | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | $\begin{gathered} \text { SR } \\ 0 \end{gathered}$ | $\begin{gathered} \mathrm{EL} \\ 1 \end{gathered}$ | ET 1 | ER | $\begin{gathered} \text { WL } \\ 0 \end{gathered}$ | WT | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 6:00 AM | CARS ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00 AM | 7 | 105 | 2 | 1 | 148 | 70 | 58 | 1 | 29 | 1 | 0 | 1 | 423 |
| 7:15 AM | 0 | 128 | 3 | 2 | 223 | 26 | 53 | 1 | 19 | 1 | 0 | 1 | 457 |
| 7:30 AM | 9 | 113 | 4 | 6 | 270 | 70 | 14 | 1 | 2 | 1 | 0 | 1 | 491 |
| 7:45 AM | 6 | 115 | 13 | 13 | 187 | 53 | 30 | 0 | 4 | 3 | 0 | 1 | 425 |
| 8:00 AM | 4 | 90 | 9 | 5 | 169 | 27 | 17 | 3 | 8 | 1 | 1 | 0 | 334 |
| 8:15 AM | 3 | 74 | 11 | 12 | 113 | 18 | 17 | 3 | 3 | 3 | 0 | 1 | 258 |
| 8:30 AM | 4 | 98 | 16 | 11 | 139 | 21 | 14 | 3 | 3 | 3 | 0 | 2 | 314 |
| 8:45 AM | 0 | 90 | 20 | 10 | 155 | 21 | 13 | 5 | 0 | 6 | 1 | 5 | 326 |
| 9:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 33 | 813 | 78 | 60 | 1404 | 306 | 216 | 17 | 68 | 19 | 2 | 12 | 3028 |
| Approach \% | 3.57 | 87.99 | 8.44 | 3.39 | 79.32 | 17.29 | 71.76 | 5.65 | 22.59 | 57.58 | 6.06 | 36.36 |  |
| App/Depart | 924 | 1 | 1041 | 1770 | 1 | 1491 | 301 | 1 | 155 | 33 | 1 | 341 |  |

AM Peak Hr Begins at: 700 AM
PEAK

| Volumes | 22 | 461 | 22 | 22 | 828 | 219 | 155 | 3 | 54 | 6 | 0 | 4 | 1796 |
| :--- | :---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

PEAK HR.
FACTOR:
0.942
$0.772 \quad \mid$
0.602 | 0.625
0.914

CONTROL: Signal
COMMENT 1:
GPS:
31.378618, -110.941097

## Intersection Turning Movement

$\xrightarrow{\stackrel{\rightharpoonup}{\text { Fineld Data Services of Arizona, Inc. }} \text {. }}$<br>520.316.6745

| N-S STREET: | Grand Ave. | DATE: 02/04/15 | LOCATION: Nogales |
| :--- | :--- | :---: | :--- |
| E-W STREET: | Produce Row | DAY: WEDNESDAY | PROJECT\# |
| 15-1041-002-Cars |  |  |  |


|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LANES: | $\begin{gathered} \mathrm{NL} \\ 1 \end{gathered}$ | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | NR 0 | $\begin{gathered} \mathrm{SL} \\ 1 \end{gathered}$ | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | SR 0 | $\begin{gathered} \mathrm{EL} \\ 1 \end{gathered}$ | ET 1 | ER 0 | $\begin{gathered} \text { WL } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WT } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 1:00 PM | CARS ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 4 | 161 | 6 | 6 | 156 | 39 | 29 | 2 | 7 | 8 | 6 | 12 | 436 |
| 4:15 PM | 10 | 148 | 5 | 7 | 133 | 31 | 27 | 2 | 6 | 6 | 2 | 7 | 384 |
| 4:30 PM | 6 | 173 | 5 | 7 | 148 | 31 | 42 | 3 | 6 | 3 | 2 | 8 | 434 |
| 4:45 PM | 1 | 129 | 5 | 1 | 118 | 16 | 25 | 2 | 5 | 4 | 2 | 5 | 313 |
| 5:00 PM | 14 | 200 | 10 | 7 | 143 | 36 | 35 | 1 | 12 | 15 | 2 | 14 | 489 |
| 5:15 PM | 10 | 156 | 2 | 1 | 135 | 34 | 46 | 0 | 14 | 9 | 3 | 12 | 422 |
| 5:30 PM | 10 | 187 | 2 | 6 | 146 | 41 | 41 | 1 | 6 | 0 | 1 | 9 | 450 |
| 5:45 PM | 10 | 156 | 1 | 10 | 134 | 38 | 32 | 2 | 7 | 8 | 2 | 11 | 411 |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 65 | 1310 | 36 | 45 | 1113 | 266 | 277 | 13 | 63 | 53 | 20 | 78 | 3339 |
| Approach \% | 4.61 | 92.84 | 2.55 | 3.16 | 78.16 | 18.68 | 78.47 | 3.68 | 17.85 | 35.10 | 13.25 | 51.66 |  |
| App/Depart | 1411 | 1 | 1665 | 1424 | I | 1229 | 353 | 1 | 94 | 151 |  | 351 |  |

PM Peak Hr Begins at: 500 PM
PEAK

| Volumes | 44 | 699 | 15 | 24 | 558 | 149 | 154 | 4 | 39 | 32 | 8 | 46 | 1772 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Approach \% | 5.80 | 92.22 | 1.98 | 3.28 | 76.33 | 20.38 | 78.17 | 2.03 | 19.80 | 37.21 | 9.30 | 53.49 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

PEAK HR.
FACTOR:

| $\mid$ | 0.846 | $\mid$ | 0.947 | $\mid$ | 0.821 | $\mid$ | 0.694 | 0.906 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

CONTROL: Signal
COMMENT 1: 0
GPS:
31.378618, -110.941097

## Project \#: 15-1041-002-H.V.

## TMC SUMMARY OF Grand Ave, \& Produce Row



Intersection Turning Movement Prepared by:

##  <br> Veracitytrafficgroup

| N-S STREET: | Grand Ave. | DATE: $02 / 04 / 15$ | LOCATION: |
| :--- | :--- | :--- | :--- |


|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LANES: | $\begin{gathered} \text { NL } \\ 1 \end{gathered}$ | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | $\begin{gathered} \text { NR } \\ 0 \end{gathered}$ | SL 1 | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | $\begin{gathered} \text { SR } \\ 0 \end{gathered}$ | $\mathrm{EL}$ | ET 1 | ER 0 | $\begin{gathered} \text { WL } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WT } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 6:00 AM | HEAVY VEHICLES ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00 AM | 0 | 5 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 7:15 AM | 0 | 4 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 6 |
| 7:30 AM | 0 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 7:45 AM | 0 | 2 | 1 | 0 | 7 | 0 | 1 | 0 | 1 | 2 | 0 | 1 | 15 |
| 8:00 AM | 0 | 4 | 1 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 11 |
| 8:15 AM | 0 | 4 | 0 | 1 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 8:30 AM | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 7 |
| 8:45 AM | 0 | 4 | 2 | 2 | 5 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 16 |
| 9:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 0 | 26 | 7 | 7 | 24 | 2 | 2 | 0 | 2 | 3 | 0 | 4 | 77 |
| Approach \% | 0.00 | 78.79 | 21.21 | 21.21 | 72.73 | 6.06 | 50.00 | 0.00 | 50.00 | 42.86 | 0.00 | 57.14 |  |
| App/Depart | 33 | 1 | 32 | 33 | 1 | 29 | 4 | 1 | 14 | 7 | 1 | 2 |  | AM Peak Hr Begins at: 800 AM

PEAK

| Volumes | 0 | 15 | 5 | 4 | 12 | 2 | 0 | 0 | 1 | 1 | 0 |
| :--- | :--- | :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach \% | 0.00 | 75.00 | 25.00 | 22.22 | 66.67 | 11.11 | 0.00 | 0.00 | 100.00 | 25.00 | 0.00 |
| 75.00 |  |  |  |  |  |  |  |  |  |  |  |

PEAK HR.
FACTOR:
0.833
0.563 | 0.250
0.500

CONTROL: Signal
COMMENT 1:
GPS:
31.378618, -110.941097

## Intersection Turning Movement

Field Data Services of Arizona, Inc.<br>520.316.6745

| N-S STREET: | Grand Ave. | DATE: 02/04/15 | LOCATION: Nogales |
| :--- | :--- | :---: | :--- |
| E-W STREET: | Produce Row | DAY: WEDNESDAY | PROJECT\# |
| 15-1041-002-H.V. |  |  |  |


| LANES: | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} \mathrm{NL} \\ 1 \end{gathered}$ | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | $\begin{gathered} \text { NR } \\ 0 \end{gathered}$ | SL | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | $\begin{gathered} \text { SR } \\ 0 \end{gathered}$ | $\begin{gathered} \mathrm{EL} \\ 1 \end{gathered}$ | $\begin{gathered} \text { ET } \\ 1 \end{gathered}$ | $\begin{gathered} \text { ER } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WL } \\ 0 \end{gathered}$ | WT | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 1:00 PM | HEAVY VEHICLES ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 3 | 8 | 2 | 5 | 8 | 3 | 0 | 0 | 1 | 2 | 0 | 3 | 35 |
| 4:15 PM | 1 | 9 | 2 | 1 | 6 | 3 | 0 | 0 | 0 | 2 | 1 | 3 | 28 |
| 4:30 PM | 1 | 6 | 4 | 4 | 7 | 3 | 3 | 1 | 2 | 4 | 0 | 2 | 37 |
| 4:45 PM | 1 | 3 | 2 | 0 | 8 | 0 | 1 | 0 | 0 | 2 | 0 | 3 | 20 |
| 5:00 PM | 2 | 12 | 7 | 5 | 9 | 1 | 0 | 0 | 4 | 2 | 0 | 1 | 43 |
| 5:15 PM | 1 | 6 | 0 | 1 | 12 | 3 | 2 | 1 | 1 | 7 | 0 | 5 | 39 |
| 5:30 PM | 2 | 12 | 5 | 2 | 10 | 0 | 3 | 0 | 3 | 6 | 0 | 3 | 46 |
| 5:45 PM | 1 | 11 | 6 | 1 | 7 | 1 | 2 | 0 | 2 | 1 | 0 | 7 | 39 |
| 6:00 PM 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 12 | 67 | 28 | 19 | 67 | 14 | 11 | 2 | 13 | 26 | 1 | 27 | 287 |
| Approach \% | 11.21 | 62.62 | 26.17 | 19.00 | 67.00 | 14.00 | 42.31 | 7.69 | 50.00 | 48.15 | 1.85 | 50.00 |  |
| App/Depart | 107 | 1 | 105 | 100 | 1 | 106 | 26 | 1 | 49 | 54 |  | 27 |  |

PM Peak Hr Begins at: 500 PM
PEAK

| Volumes | 6 | 41 | 18 | 9 | 38 | 5 | 7 | 1 | 10 | 16 | 0 | 16 | 167 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | | Approach \% | 9.23 | 63.08 | 27.69 | 17.31 | 73.08 | 9.62 | 38.89 | 5.56 | 55.56 | 50.00 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

PEAK HR.
FACTOR:

| $\mid$ | 0.774 | $\mid$ | 0.813 | $\mid$ | 0.750 | $\mid$ | 0.667 | 0.908 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

CONTROL: Signal
COMMENT 1: 0
GPS:
31.378618, -110.941097

## Intersection Turning Movement

## Prepared by:

Field Data Services of Arizona, Inc.


Intersection Turning Movement
Prepared by:

## $\xrightarrow{\stackrel{\rightharpoonup}{\mid}} \stackrel{\text { Dield Data Services of Arizona, Inc. }}{520.316 .6745}$ <br> Veracitytrafficgroup

N-S STREET: Grand Ave.
DATE: 02/04/15
LOCATION: Nogales
E-W STREET: Calle Sonora
DAY: WEDNESDAY
PROJECT\# 15-1041-003 - Cars

|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LANES: | $\begin{gathered} \mathrm{NL} \\ 2 \end{gathered}$ | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | $\begin{gathered} \text { NR } \\ 0 \end{gathered}$ | SL 1 | ST | $\begin{gathered} \mathrm{SR} \\ 1 \end{gathered}$ | $\begin{gathered} \mathrm{EL} \\ 2 \end{gathered}$ | ET 1 | ER 1 | $\begin{gathered} \text { WL } \\ 0 \end{gathered}$ | WT | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 6:00 AM | CARS ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00 AM | 28 | 85 | 1 | 9 | 92 | 61 | 42 | 10 | 32 | 8 | 11 | 8 | 387 |
| 7:15 AM | 30 | 88 | 6 | 8 | 106 | 62 | 37 | 21 | 69 | 11 | 21 | 5 | 464 |
| 7:30 AM | 64 | 95 | 4 | 6 | 177 | 53 | 31 | 6 | 36 | 18 | 29 | 7 | 526 |
| 7:45 AM | 71 | 91 | 9 | 11 | 123 | 63 | 47 | 20 | 48 | 20 | 48 | 12 | 563 |
| 8:00 AM | 37 | 88 | 7 | 16 | 115 | 35 | 33 | 10 | 34 | 3 | 8 | 9 | 395 |
| 8:15 AM | 50 | 71 | 9 | 6 | 88 | 40 | 35 | 9 | 41 | 8 | 22 | 4 | 383 |
| 8:30 AM | 46 | 82 | 4 | 9 | 84 | 48 | 49 | 11 | 30 | 12 | 18 | 7 | 400 |
| 8:45 AM | 44 | 77 | 12 | 12 | 92 | 56 | 39 | 13 | 38 | 12 | 18 | 6 | 419 |
| 9:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 370 | 677 | 52 | 77 | 877 | 418 | 313 | 100 | 328 | 92 | 175 | 58 | 3537 |
| Approach \% | 33.67 | 61.60 | 4.73 | 5.61 | 63.92 | 30.47 | 42.24 | 13.50 | 44.26 | 28.31 | 53.85 | 17.85 |  |
| App/Depart | 1099 | 1 | 1048 | 1372 | 1 | 1297 | 741 | 1 | 229 | 325 | 1 | 963 |  |

AM Peak Hr Begins at: 715 AM
PEAK

| Volumes | 202 | 362 | 26 | 41 | 521 | 213 | 148 | 57 | 187 | 52 | 106 | 33 | 1948 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Approach \% | 34.24 | 61.36 | 4.41 | 5.29 | 67.23 | 27.48 | 37.76 | 14.54 | 47.70 | 27.23 | 55.50 | 17.28 |  |

PEAK HR.
FACTOR:
0.863
0.821 |
0.772
0.597
0.865

CONTROL: Signal
COMMENT 1:
GPS:
31.367221,-110.931068

## Intersection Turning Movement

$\xrightarrow{\text { Field Data Services of Arizona, Inc. }}$<br>520.316.6745

| N-S STREET: | Grand Ave. | DATE: 02/04/15 | LOCATION: Nogales |
| :--- | :--- | :---: | :--- |
| E-W STREET: | Calle Sonora | DAY: WEDNESDAY | PROJECT\# |
| 15-1041-003-Cars |  |  |  |


| LANES: | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NL 2 | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | NR 0 | SL 1 | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | $\begin{gathered} \text { SR } \\ 1 \end{gathered}$ | $\begin{gathered} \mathrm{EL} \\ 2 \end{gathered}$ | ET 1 | $\begin{gathered} \text { ER } \\ 1 \end{gathered}$ | WL 0 | $\begin{gathered} \text { WT } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 1:00 PM | CARS ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 77 | 108 | 16 | 11 | 126 | 60 | 75 | 36 | 70 | 16 | 27 | 24 | 646 |
| 4:15 PM | 75 | 114 | 21 | 14 | 97 | 57 | 51 | 26 | 62 | 13 | 17 | 6 | 553 |
| 4:30 PM | 74 | 100 | 11 | 9 | 100 | 61 | 79 | 26 | 81 | 9 | 22 | 13 | 585 |
| 4:45 PM | 92 | 98 | 19 | 19 | 93 | 42 | 69 | 29 | 71 | 6 | 24 | 6 | 568 |
| 5:00 PM | 91 | 160 | 21 | 21 | 132 | 34 | 72 | 31 | 69 | 7 | 31 | 29 | 698 |
| 5:15 PM | 87 | 119 | 12 | 23 | 120 | 34 | 102 | 25 | 80 | 16 | 21 | 14 | 653 |
| 5:30 PM | 77 | 109 | 4 | 8 | 99 | 49 | 80 | 26 | 52 | 11 | 22 | 13 | 550 |
| 5:45 PM | 80 | 137 | 9 | 13 | 133 | 54 | 91 | 32 | 61 | 8 | 19 | 11 | 648 |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 653 | 945 | 113 | 118 | 900 | 391 | 619 | 231 | 546 | 86 | 183 | 116 | 4901 |
| Approach \% | 38.16 | 55.23 | 6.60 | 8.37 | 63.88 | 27.75 | 44.34 | 16.55 | 39.11 | 22.34 | 47.53 | 30.13 |  |
|  |  | 1711 | 1 | 1680 | 1409 | 1 | 1532 | 1396 | 1 | 462 | 385 | 1 | 1227 |

PM Peak Hr Begins at: 500 PM
PEAK

| Volumes | 335 | 525 | 46 | 65 | 484 | 171 | 345 | 114 | 262 | 42 | 93 | 67 | 2549 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Approach \% | 36.98 | 57.95 | 5.08 | 9.03 | 67.22 | 23.75 | 47.85 | 15.81 | 36.34 | 20.79 | 46.04 | 33.17 |  |

PEAK HR.
FACTOR:

CONTROL: Signal
COMMENT 1: 0
GPS:
31.367221, -110.931068

Project \#: $15-1041-003$ - H.V.

## TMC SUMMARY OF Grand Ave, \& Calle Sonora



| AM PEAK HOUR | 800 AM |
| :--- | :---: |
| NOON PEAK HOUR |  |
| PM PEAK HOUR | 500 PM |

Intersection Turning Movement Prepared by:

##  <br> Veracitytrafficgroup

| N-S STREET: | Grand Ave. | DATE: $02 / 04 / 15$ | LOCATION: |
| :--- | :--- | :--- | :--- |


|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LANES: | $\begin{gathered} \mathrm{NL} \\ 2 \end{gathered}$ | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | $\begin{gathered} \text { NR } \\ 0 \end{gathered}$ | SL 1 | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | SR | $\begin{gathered} \mathrm{EL} \\ 2 \end{gathered}$ | ET 1 | ER 1 | $\begin{gathered} \text { WL } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WT } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 6:00 AM | HEAVY VEHICLES ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00 AM | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 2 | 1 | 0 | 0 | 0 | 4 |
| 7:15 AM | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 7:30 AM | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 5 |
| 7:45 AM | 0 | 1 | 0 | 0 | 3 | 5 | 3 | 0 | 1 | 0 | 2 | 0 | 15 |
| 8:00 AM | 1 | 0 | 1 | 1 | 2 | 2 | 2 | 0 | 2 | 0 | 1 | 1 | 13 |
| 8:15 AM | 1 | 0 | 0 | 2 | 0 | 1 | 3 | 2 | 0 | 0 | 0 | 1 | 10 |
| 8:30 AM | 1 | 2 | 0 | 0 | 0 | 2 | 3 | 1 | 0 | 0 | 2 | 0 | 11 |
| 8:45 AM | 3 | 1 | 1 | 1 | 0 | 6 | 4 | 1 | 1 | 0 | 2 | 1 | 21 |
| 9:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 8 | 5 | 2 | 6 | 5 | 18 | 15 | 8 | 5 | 0 | 7 | 3 | 82 |
| Approach \% | 53.33 | 33.33 | 13.33 | 20.69 | 17.24 | 62.07 | 53.57 | 28.57 | 17.86 | 0.00 | 70.00 | 30.00 |  |
| App/Depart | 15 | 1 | 23 | 29 | 1 | 10 | 28 | 1 | 16 | 10 | 1 | 33 |  |

AM Peak Hr Begins at: 800 AM
PEAK

| Volumes | 6 | 3 | 2 | 4 | 2 | 11 | 12 | 4 | 3 | 0 | 5 | 3 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach \% | 54.55 | 27.27 | 18.18 | 23.53 | 11.76 | 64.71 | 63.16 | 21.05 | 15.79 | 0.00 | 62.50 | 37.50 |

PEAK HR.
FACTOR:
0.550
$0.607 \quad \mid$
0.792
0.667
0.655

CONTROL: Signal
COMMENT 1:
GPS:
31.367221, -110.931068

## Intersection Turning Movement

$\xrightarrow{\text { Field Data Services of Arizona, Inc. }}$<br>520.316.6745

| N-S STREET: | Grand Ave. | DATE: 02/04/15 | LOCATION: Nogales |
| :--- | :--- | :---: | :--- |
| E-W STREET: | Calle Sonora | DAY: WEDNESDAY | PROJECT\# |
| 15-1041-003-H.V. |  |  |  |


|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LANES: | $\mathrm{NL}$ | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | $\begin{gathered} \text { NR } \\ 0 \end{gathered}$ | SL | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | SR | $\begin{gathered} \mathrm{EL} \\ 2 \end{gathered}$ | ET | ER | $\begin{gathered} \text { WL } \\ 0 \end{gathered}$ | WT | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 1:00 PM | HEAVY VEHICLES ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 1 | 1 | 0 | 0 | 3 | 7 | 15 | 3 | 0 | 0 | 1 | 3 | 34 |
| 4:15 PM | 1 | 1 | 0 | 2 | 0 | 7 | 11 | 2 | 1 | 0 | 2 | 2 | 29 |
| 4:30 PM | 2 | 2 | 0 | 2 | 1 | 9 | 15 | 0 | 2 | 0 | 3 | 0 | 36 |
| 4:45 PM | 1 | 1 | 0 | 0 | 1 | 11 | 10 | 3 | 1 | 0 | 5 | 1 | 34 |
| 5:00 PM | 1 | 3 | 0 | 4 | 6 | 5 | 15 | 2 | 1 | 0 | 2 | 3 | 42 |
| 5:15 PM | 2 | 1 | 0 | 2 | 6 | 8 | 12 | 4 | 1 | 0 | 1 | 1 | 38 |
| 5:30 PM | 2 | 1 | 0 | 3 | 3 | 13 | 9 | 0 | 1 | 0 | 2 | 6 | 40 |
| 5:45 PM | 5 | 2 | 0 | 2 | 2 | 8 | 15 | 3 | 2 | 0 | 1 | 1 | 41 |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 15 | 12 | 0 | 15 | 22 | 68 | 102 | 17 | 9 | 0 | 17 | 17 | 294 |
| Approach \% | 55.56 | 44.44 | 0.00 | 14.29 | 20.95 | 64.76 | 79.69 | 13.28 | 7.03 | 0.00 | 50.00 | 50.00 |  |
| App/Depart | 27 | I | 131 | 105 | 1 | 31 | 128 | 1 | 32 | 34 |  | 100 |  |

PM Peak Hr Begins at: 500 PM
PEAK

| Volumes | 10 | 7 | 0 | 11 | 17 | 34 | 51 | 9 | 5 | 0 | 6 | 11 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach \% | 58.82 | 41.18 | 0.00 | 17.74 | 27.42 | 54.84 | 78.46 | 13.85 | 7.69 | 0.00 | 35.29 | 64.71 |

PEAK HR.
FACTOR:

CONTROL: Signal
COMMENT 1: 0
GPS:
31.367221, -110.931068

Intersection Turning Movement Prepared by:
Field Data Services of Arizona, Inc.

## Project \#: 15-1041-004-Cars

TMC SUMMARY OF Smokey Ln, \& Calle Sonora

Calle Sonora


Calle Sonora
$\qquad$


| LOCATION \#: 15-1041-004-Cars |  |  |
| :---: | :---: | :---: |
| TURNING MOVEMENT COUNT |  |  |
| Smokey Ln. \& Calle Sonora |  |  |
| (Intersection Name) |  |  |
| WEDNESDAY |  | 02/04/1.5 |
| Day |  | Date |
| COUNT PERIODS |  |  |
| AM | 700AM | 900AM |
| NOON |  |  |
| PM | 400PM | 600PM |

Intersection Turning Movement Prepared by:

##  <br> Veracitytrafficgroup

| N-S STREET: | Smokey Ln. | DATE: 02/04/15 | LOCATION: Nogales |
| :--- | :--- | :--- | :--- |
| E-W STREET: | Calle Sonora | DAY: WEDNESDAY | PROJECT\# |
| 15-1041-004-Cars |  |  |  |


|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| LANES: | 2 | 2 | 0 | 1 | 2 | 1 | 2 | 1 | 1 | 0 | 1 | , |  |



| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 34 | 13 | 38 | 3 | 4 | 15 | 36 | 108 | 54 | 86 | 257 | 12 | 660 |
| Approach \% | 40.00 | 15.29 | 44.71 | 13.64 | 18.18 | 68.18 | 18.18 | 54.55 | 27.27 | 24.23 | 72.39 | 3.38 |  |
| App/Depart | 85 | 1 | 61 | 22 | 1 | 144 | 198 | 1 | 149 | 355 | 1 | 306 |  |

AM Peak Hr Begins at: 700 AM
PEAK

| Volumes | 15 | 5 | 21 | 0 | 2 | 5 | 14 | 57 | 26 | 57 | 172 | 8 | 382 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |


| Approach \% | 36.59 | 12.20 | 51.22 | 0.00 | 28.57 | 71.43 | 14.43 | 58.76 | 26.80 | 24.05 | 72.57 | 3.38 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

PEAK HR.
FACTOR:
0.788
$0.583 \quad \mid$
0.782
0.554
0.637

CONTROL: 2-Way Stop (NB \& SB)
COMMENT 1:
GPS:
31.367234, -110.929419

## Intersection Turning Movement

|  | Data Services of Arizona, Inc. $\underset{520.316 .6745}{ } \mathcal{Y}^{\text {An }}$ veracitytrafficgroup |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| N-S STREET: <br> E-W STREET: | Smokey Ln. |  |  |  | DATE: 02/04/15 |  |  |  | LOCATION: Nogales |  |  |  |  |
|  | Calle Sonora |  |  |  | DAY: WEDNESDAY |  |  |  | PROJECT\# |  | 15-1041-004-Cars |  |  |
|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  |  |
| LANES: | $\begin{gathered} \mathrm{NL} \\ 2 \end{gathered}$ | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | $\begin{gathered} \text { NR } \\ 0 \end{gathered}$ | $\begin{gathered} \mathrm{SL} \\ 1 \end{gathered}$ | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | SR | $\begin{gathered} \mathrm{EL} \\ 2 \end{gathered}$ | ET 1 | $\mathrm{ER}$ | $\begin{gathered} \text { WL } \\ 0 \end{gathered}$ | WT | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ | TOTAL |
| 1:00 PM | CARS ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4:00 PM | 19 | 2 | 16 | 0 | 1 | 4 | 4 | 26 | 16 | 14 | 33 | 1 | 136 |
| 4:15 PM | 12 | 3 | 15 | 0 | 0 | 8 | 5 | 41 | 11 | 5 | 20 | 1 | 121 |
| 4:30 PM | 17 | 0 | 12 | 0 | 1 | 9 | 3 | 42 | 19 | 11 | 26 | 0 | 140 |
| 4:45 PM | 2 | 0 | 16 | 0 | 4 | 2 | 4 | 30 | 11 | 15 | 26 | 0 | 110 |
| 5:00 PM | 17 | 1 | 13 | 1 | 2 | 7 | 5 | 62 | 15 | 22 | 39 | 0 | 184 |
| 5:15 PM | 6 | 1 | 7 | 0 | 0 | 6 | 4 | 34 | 14 | 12 | 33 | 2 | 119 |
| 5:30 PM | 10 | 0 | 18 | 0 | 0 | 8 | 5 | 24 | 15 | 21 | 33 | 0 | 134 |
| 5:45 PM | 2 | 1 | 9 | 0 | 1 | 4 | 2 | 25 | 17 | 14 | 20 | 0 | 95 |
| 6:00 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 85 | ${ }^{8} 8.02$ | 106 | $\begin{aligned} & \hline 1 \\ & 1.72 \end{aligned}$ | $\begin{gathered} 9 \\ 15.52 \end{gathered}$ | $\begin{array}{c\|} \hline 48 \\ 82.76 \end{array}$ | $\begin{aligned} & 32 \\ & 7.37 \\ & \hline \end{aligned}$ | $\begin{gathered} 284 \\ 65.44 \end{gathered}$ | $\begin{array}{l\|} \hline 118 \\ 27.19 \end{array}$ | $\begin{aligned} & \hline 114 \\ & 32.76 \end{aligned}$ | $\begin{gathered} \hline 230 \\ 66.09 \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 4 \\ & 1.15 \end{aligned}$ | 1039 |
| Approach \% | 42.71 |  | 53.27 |  |  |  |  |  |  |  |  |  |  |
| App/Depart | 199 | 1 | 44 | 58 | 1 | 241 | 434 | 1 | 391 | 348 | 1 | 363 |  |

PM Peak Hr Begins at: 415 PM
PEAK

| Volumes | 48 | 4 | 56 | 1 | 7 | 26 | 17 | 175 | 56 | 53 | 111 | 1 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 555 |  |  |  |  |  |  |  |  |  |  |  |  |


| Approach \% | 44.44 | 3.70 | 51.85 | 2.94 | 20.59 | 76.47 | 6.85 | 70.56 | 22.58 | 32.12 | 67.27 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |

PEAK HR.
FACTOR:
CONTROL: 2-Way Stop (NB \& SB)
COMMENT 1: 0
GPS:
31.367234, -110.929419

Intersection Turning Movement

## Prepared by:

Field Data Services of Arizona, Inc.

## Project \#: 15-1041-004-H.V.

## TMC SUMMARY OF Smokev Ln. \& Calle Sonora

Calle Sonora



Calle Sonora
$\qquad$


LOCATION \#: 15-1041-004-H.V.

TURNING MOVEMENT COUNT

Smokey Ln. \& Calle Sonora (Intersection Name)
$\qquad$
Day
02/04/15 Date

| COUNT PERIODS |  |  |  |
| :---: | :---: | :--- | :---: |
| AM | 700 AM | - | 900 AM |
| NOON |  | - |  |
| PM | 400 PM | - | 600 PM |

Intersection Turning Movement Prepared by:

##  <br> Veracitytrafficgroup

N-S STREET: Smokey Ln.
DATE: 02/04/15
LOCATION: Nogales
E-W STREET: Calle Sonora
DAY: WEDNESDAY
PROJECT\# 15-1041-004-H.V.

|  | NORTHBOUND |  |  | SOUTHBOUND |  |  | EASTBOUND |  |  | WESTBOUND |  |  | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LANES: | $\begin{gathered} \mathrm{NL} \\ 2 \end{gathered}$ | $\begin{gathered} \text { NT } \\ 2 \end{gathered}$ | $\begin{gathered} \text { NR } \\ 0 \end{gathered}$ | SL 1 | $\begin{gathered} \text { ST } \\ 2 \end{gathered}$ | $\begin{gathered} \text { SR } \\ 1 \end{gathered}$ | $\begin{gathered} \mathrm{EL} \\ 2 \end{gathered}$ | ET 1 | ER 1 | $\begin{gathered} \text { WL } \\ 0 \end{gathered}$ | $\begin{gathered} \text { WT } \\ 1 \end{gathered}$ | $\begin{gathered} \text { WR } \\ 0 \end{gathered}$ |  |
| 6:00 AM | HEAVY VEHICLES ONLY |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7:00 AM | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 4 |
| 7:15 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 2 |
| 7:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 |
| 7:45 AM | 1 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 3 |
| 8:00 AM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 3 |
| 8:15 AM | 1 | 0 | 0 | 0 | 1 | 1 | 1 | 0 | 1 | 0 | 1 | 0 | 6 |
| 8:30 AM | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 2 | 0 | 1 | 0 | 5 |
| 8:45 AM | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 5 |
| 9:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:00 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:15 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11:45 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |


| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 7 | 00.00 | 0 | 0 | 1 | 3 | 6 | 3 | 6 | 0 | 4 | 0 | 30 |
| Approach \% | 100.00 |  | 0.00 | 0.00 | 25.00 | 75.00 | 40.00 | 20.00 | 40.00 | 0.00 | 100.00 | 0.00 |  |
| App/Depart | 7 | 1 | 6 | 4 | 1 | 7 | 15 | 1 | 3 | 4 | 1 | 14 |  |

AM Peak Hr Begins at: 800 AM
PEAK

| Volumes | 3 | 0 | 0 | 0 | 1 | 2 | 2 | 2 | 5 | 0 | 4 | 0 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach \% | 100.00 | 0.00 | 0.00 | 0.00 | 33.33 | 66.67 | 22.22 | 22.22 | 55.56 | 0.00 | 100.00 | 0.00 |

PEAK HR.
FACTOR:
0.750
0.375
0.750
0.500
0.792

CONTROL: 2-Way Stop (NB \& SB)
COMMENT 1:
GPS:
31.367234, -110.929419

## Intersection Turning Movement



| TOTAL | NL | NT | NR | SL | ST | SR | EL | ET | ER | WL | WT | WR | TOTAL |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Volumes | 5 | 2 | 0 | 1 | 1 | 20 | 20 | 9 | 1 | 1 | 10 | 0 | 70 |
| Approach \% | 71.43 | 28.57 | 0.00 | 4.55 | 4.55 | 90.91 | 66.67 | 30.00 | 3.33 | 9.09 | 90.91 | 0.00 |  |
| App/Depart | 7 | 1 | 22 | 22 | / | 3 | 30 | 1 | 10 | 11 | / | 35 |  |

PM Peak Hr Begins at: 500 PM
PEAK

| Volumes | 1 | 0 | 0 | 0 | 0 | 12 | 15 | 3 | 1 | 0 | 4 | 0 | 36 |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach \% | 100.00 | 0.00 | 0.00 | 0.00 | 0.00 | 100.00 | 78.95 | 15.79 | 5.26 | 0.00 | 100.00 | 0.00 |  |

Approach \%
.

PEAK HR.
FACTOR

CONTROL: 2-Way Stop (NB \& SB)
COMMENT 1: 0
GPS: 31.367234,-110.929419

Gold Hill Rd. east of Grand Ave (on bridge)


Gold Hill Rd. east of Grand Ave (on bridge)

| WB Latitude: 0 ' 0.000 Undefined |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start |  | Cars \& | 2 Axle |  | 2 Axle | 3 Axle | 4 Axle | <5 Axle | 5 Axle | >6 Axle | <6 Axle | 6 Axle | >6 Axle |  |
| Time | Bikes | Tlrs | Long | Buses | 6 Tire | Single | Single | Double | Double | Double | Multi | Multi | Multi | Total |
| 2/4/15 | 0 | 11 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 |
| 01:00 | 1 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 02:00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 3 |
| 03:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 04:00 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 05:00 | 0 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 06:00 | 1 | 31 | 8 | 0 | 1 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 45 |
| 07:00 | 1 | 42 | 24 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 72 |
| 08:00 | 0 | 43 | 15 | 0 | 0 | 1 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 62 |
| 09:00 | 0 | 37 | 12 | 0 | 3 | 5 | 0 | 0 | 2 | 0 | 0 | 0 | 1 | 60 |
| 10:00 | 1 | 48 | 23 | 1 | 5 | 2 | 0 | 1 | 1 | 1 | 0 | 1 | 0 | 84 |
| 11:00 | 2 | 57 | 21 | 0 | 10 | 3 | 1 | 0 | 13 | 1 | 0 | 0 | 3 | 111 |
| 12 PM | 2 | 61 | 30 | 2 | 6 | 5 | 2 | 0 | 5 | 0 | 0 | 0 | 1 | 114 |
| 13:00 | 3 | 68 | 31 | 1 | 8 | 1 | 4 | 1 | 12 | 1 | 0 | 1 | 4 | 135 |
| 14:00 | 3 | 51 | 35 | 2 | 5 | 5 | 3 | 1 | 8 | 0 | 0 | 0 | 1 | 114 |
| 15:00 | 3 | 58 | 31 | 0 | 5 | 3 | 2 | 1 | 5 | 0 | 0 | 1 | 3 | 112 |
| 16:00 | 4 | 71 | 18 | 0 | 1 | 0 | 0 | 1 | 3 | 1 | 0 | 1 | 2 | 102 |
| 17:00 | 7 | 79 | 32 | 3 | 5 | 5 | 1 | 0 | 4 | 0 | 0 | 1 | 2 | 139 |
| 18:00 | 6 | 37 | 12 | 3 | 9 | 5 | 3 | 1 | 4 | 1 | 0 | 1 | 3 | 85 |
| 19:00 | 5 | 38 | 8 | 1 | 4 | 3 | 2 | 0 | 11 | 1 | 0 | 0 | 0 | 73 |
| 20:00 | 4 | 31 | 11 | 1 | 4 | 4 | 0 | 0 | 8 | 1 | 0 | 0 | 1 | 65 |
| 21:00 | 3 | 26 | 8 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 40 |
| 22:00 | 4 | 30 | 6 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 43 |
| 23:00 | 0 | 6 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| Day | 50 | 838 | 341 | 15 | 71 | 46 | 22 | 6 | 81 | 7 | 0 | 7 | 21 | 1505 |
| Percent | 3.3\% | 55.7\% | 22.7\% | 1.0\% | 4.7\% | 3.1\% | 1.5\% | 0.4\% | 5.4\% | 0.5\% | 0.0\% | 0.5\% | 1.4\% |  |
| AM Peak | 11:00 | 11:00 | 07:00 | 01:00 | 11:00 | 09:00 | 08:00 | 10:00 | 11:00 | 10:00 |  | 07:00 | 11:00 | 11:00 |
| Vol. | 2 | 57 | 24 | 1 | 10 | 5 | 2 | 1 | 13 | 1 |  | 1 | 3 | 111 |
| PM Peak | 17:00 | 17:00 | 14:00 | 17:00 | 18:00 | 12:00 | 13:00 | 13:00 | 13:00 | 13:00 |  | 13:00 | 13:00 | 17:00 |
| Vol. | 7 | 79 | 35 | 3 | 9 | 5 | 4 | 1 | 12 | 1 |  | 1 | 4 | 139 |
| Grand Total | 50 | 838 | 341 | 15 | 71 | 46 | 22 | 6 | 81 | 7 | 0 | 7 | 21 | 1505 |
| Percent | 3.3\% | 55.7\% | 22.7\% | 1.0\% | 4.7\% | 3.1\% | 1.5\% | 0.4\% | 5.4\% | 0.5\% | 0.0\% | 0.5\% | 1.4\% |  |

Gold Hill Rd. east of Grand Ave (on bridge)

| EB, WB |  |  |  |  |  |  |  |  |  |  |  | (on bridge) <br> Latitude: 0' 0.000 Undefined |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start |  | Cars \& | 2 Axle |  | 2 Axle | 3 Axle | 4 Axle | <5 Axle | 5 Axle | >6 Axle | <6 Axle | 6 Axle | >6 Axle |  |
| Time | Bikes | Tlrs | Long | Buses | 6 Tire | Single | Single | Double | Double | Double | Multi | Multi | Multi | Total |
| 2/4/15 | 0 | 18 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 25 |
| 01:00 | 1 | 5 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 02:00 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 4 |
| 03:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 2 |
| 04:00 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| 05:00 | 1 | 14 | 4 | 0 | 1 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 22 |
| 06:00 | 1 | 55 | 21 | 0 | 3 | 2 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 86 |
| 07:00 | 4 | 66 | 55 | 1 | 4 | 2 | 1 | 0 | 0 | 0 | 0 | 1 | 0 | 134 |
| 08:00 | 0 | 79 | 55 | 0 | 1 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 1 | 141 |
| 09:00 | 2 | 84 | 65 | 0 | 3 | 8 | 2 | 0 | 7 | 1 | 0 | 0 | 3 | 175 |
| 10:00 | 5 | 98 | 64 | 4 | 11 | 5 | 1 | 1 | 1 | 1 | 0 | 2 | 1 | 194 |
| 11:00 | 3 | 108 | 53 | 1 | 15 | 6 | 4 | 1 | 18 | 2 | 0 | 2 | 7 | 220 |
| 12 PM | 6 | 104 | 68 | 5 | 16 | 11 | 4 | 2 | 8 | 2 | 0 | 1 | 6 | 233 |
| 13:00 | 7 | 120 | 77 | 3 | 11 | 8 | 10 | 4 | 14 | 3 | 1 | 2 | 7 | 267 |
| 14:00 | 7 | 99 | 89 | 6 | 11 | 10 | 5 | 2 | 9 | 1 | 0 | 3 | 3 | 245 |
| 15:00 | 12 | 96 | 67 | 1 | 9 | 16 | 8 | 1 | 6 | 1 | 2 | 2 | 3 | 224 |
| 16:00 | 11 | 118 | 50 | 3 | 5 | 1 | 2 | 2 | 4 | 1 | 0 | 1 | 6 | 204 |
| 17:00 | 11 | 124 | 65 | 9 | 7 | 6 | 2 | 0 | 5 | 0 | 1 | 2 | 7 | 239 |
| 18:00 | 11 | 68 | 38 | 5 | 18 | 11 | 10 | 3 | 11 | 4 | 0 | 3 | 6 | 188 |
| 19:00 | 6 | 69 | 25 | 4 | 10 | 4 | 6 | 0 | 14 | 2 | 0 | 0 | 2 | 142 |
| 20:00 | 6 | 57 | 23 | 1 | 5 | 5 | 0 | 0 | 9 | 2 | 1 | 1 | 3 | 113 |
| 21:00 | 3 | 42 | 20 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 68 |
| 22:00 | 4 | 35 | 12 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 54 |
| 23:00 | 0 | 7 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| Day Total | 101 | 1468 | 870 | 44 | 132 | 100 | 60 | 17 | 113 | 20 | 5 | 21 | 55 | 3006 |
| Percent | 3.4\% | 48.8\% | 28.9\% | 1.5\% | 4.4\% | 3.3\% | 2.0\% | 0.6\% | 3.8\% | 0.7\% | 0.2\% | 0.7\% | 1.8\% |  |
| AM Peak | 10:00 | 11:00 | 09:00 | 10:00 | 11:00 | 09:00 | 11:00 | 05:00 | 11:00 | 11:00 |  | 10:00 | 11:00 | 11:00 |
| Vol. | 5 | 108 | 65 | 4 | 15 | 8 | 4 | 1 | 18 | 2 |  | 2 | 7 | 220 |
| PM Peak | 15:00 | 17:00 | 14:00 | 17:00 | 18:00 | 15:00 | 13:00 | 13:00 | 13:00 | 18:00 | 15:00 | 14:00 | 13:00 | 13:00 |
| Vol. | 12 | 124 | 89 | 9 | 18 | 16 | 10 | 4 | 14 | 4 | 2 | 3 | 7 | 267 |
| Grand Total | 101 | 1468 | 870 | 44 | 132 | 100 | 60 | 17 | 113 | 20 | 5 | 21 | 55 | 3006 |
| Percent | 3.4\% | 48.8\% | 28.9\% | 1.5\% | 4.4\% | 3.3\% | 2.0\% | 0.6\% | 3.8\% | 0.7\% | 0.2\% | 0.7\% | 1.8\% |  |


| EB Latitude: 0 ' 0.000 Undefined |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start |  | Cars \& | 2 Axle |  | 2 Axle | 3 Axle | 4 Axle | <5 Axle | 5 Axle | >6 Axle | <6 Axle | 6 Axle | >6 Axle |  |
| Time | Bikes | TIrs | Long | Buses | 6 Tire | Single | Single | Double | Double | Double | Multi | Multi | Multi | Total |
| 2/4/15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 02:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 03:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:00 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 8 |
| 05:00 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 3 |
| 06:00 | 0 | 9 | 0 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 12 |
| 07:00 | 1 | 51 | 15 | 2 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 73 |
| 08:00 | 2 | 72 | 14 | 0 | 2 | 0 | 1 | 1 | 2 | 3 | 0 | 0 | 0 | 97 |
| 09:00 | 5 | 73 | 17 | 0 | 2 | 1 | 1 | 2 | 2 | 0 | 0 | 0 | 2 | 105 |
| 10:00 | 3 | 56 | 14 | 4 | 10 | 2 | 1 | 2 | 4 | 4 | 0 | 0 | 3 | 103 |
| 11:00 | 8 | 49 | 13 | 1 | 6 | 4 | 1 | 1 | 10 | 1 | 0 | 1 | 2 | 97 |
| 12 PM | 3 | 39 | 7 | 2 | 7 | 5 | 0 | 0 | 7 | 0 | 0 | 1 | 3 | 74 |
| 13:00 | 4 | 17 | 8 | 9 | 5 | 1 | 3 | 1 | 7 | 0 | 0 | 0 | 4 | 59 |
| 14:00 | 6 | 22 | 6 | 5 | 6 | 3 | 2 | 1 | 3 | 1 | 0 | 0 | 0 | 55 |
| 15:00 | 1 | 26 | 12 | 3 | 4 | 0 | 0 | 0 | 11 | 2 | 1 | 0 | 2 | 62 |
| 16:00 | 5 | 33 | 3 | 3 | 3 | 3 | 3 | 3 | 5 | 4 | 3 | 2 | 1 | 71 |
| 17:00 | 3 | 36 | 6 | 2 | 2 | 3 | 5 | 1 | 3 | 2 | 0 | 0 | 1 | 64 |
| 18:00 | 4 | 13 | 3 | 1 | 3 | 1 | 1 | 1 | 5 | 2 | 0 | 0 | 2 | 36 |
| 19:00 | 0 | 1 | 1 | 2 | 0 | 2 | 0 | 0 | 3 | 1 | 0 | 0 | 0 | 10 |
| 20:00 | 2 | 2 | 0 | 0 | 0 | 1 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 7 |
| 21:00 | 1 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 5 |
| 22:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 23:00 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| $\begin{aligned} & \text { Day } \\ & \text { Total } \end{aligned}$ | 48 | 507 | 122 | 34 | 53 | 26 | 18 | 15 | 70 | 21 | 4 | 4 | 21 | 943 |
| Percent | 5.1\% | 53.8\% | 12.9\% | 3.6\% | 5.6\% | 2.8\% | 1.9\% | 1.6\% | 7.4\% | 2.2\% | 0.4\% | 0.4\% | 2.2\% |  |
| AM Peak | 11:00 | 09:00 | 09:00 | 10:00 | 10:00 | 11:00 | 08:00 | 09:00 | 11:00 | 10:00 |  | 11:00 | 10:00 | 09:00 |
| Vol. | 8 | 73 | 17 | 4 | 10 | 4 | 1 | 2 | 10 | 4 |  | 1 | 3 | 105 |
| PM Peak | 14:00 | 12:00 | 15:00 | 13:00 | 12:00 | 12:00 | 17:00 | 16:00 | 15:00 | 16:00 | 16:00 | 16:00 | 13:00 | 12:00 |
| Vol. | 6 | 39 | 12 | 9 | 7 | 5 | 5 | 3 | 11 | 4 | 3 | 2 | 4 | 74 |
| Grand Total | 48 | 507 | 122 | 34 | 53 | 26 | 18 | 15 | 70 | 21 | 4 | 4 | 21 | 943 |
| Percent | 5.1\% | 53.8\% | 12.9\% | 3.6\% | 5.6\% | 2.8\% | 1.9\% | 1.6\% | 7.4\% | 2.2\% | 0.4\% | 0.4\% | 2.2\% |  |


| Start <br> Time | Bikes | Cars \& Tlrs | 2 Axle Long | Buses | 2 Axle 6 Tire | 3 Axle Single | 4 Axle Single | $<5$ Axle Double | 5 Axle Double | >6 Axle Double | $<6$ Axle Multi | 6 Axle Multi | $>6 \text { Axle }$ Multi | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2/4/15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 02:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 03:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:00 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:00 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 06:00 | 2 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| 07:00 | 1 | 10 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 14 |
| 08:00 | 3 | 14 | 4 | 0 | 2 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 26 |
| 09:00 | 9 | 56 | 14 | 5 | 5 | 2 | 1 | 0 | 3 | 0 | 0 | 2 | 2 | 99 |
| 10:00 | 5 | 52 | 19 | 2 | 3 | 3 | 4 | 0 | 5 | 0 | 0 | 2 | 1 | 96 |
| 11:00 | 3 | 62 | 9 | 5 | 7 | 5 | 0 | 0 | 1 | 4 | 0 | 1 | 4 | 101 |
| 12 PM | 3 | 40 | 15 | 5 | 4 | 9 | 1 | 1 | 0 | 1 | 0 | 1 | 4 | 84 |
| 13:00 | 5 | 28 | 6 | 4 | 6 | 7 | 1 | 0 | 5 | 1 | 0 | 0 | 6 | 69 |
| 14:00 | 2 | 31 | 6 | 9 | 3 | 6 | 4 | 1 | 2 | 1 | 0 | 3 | 5 | 73 |
| 15:00 | 6 | 40 | 5 | 6 | 9 | 6 | 6 | 0 | 3 | 0 | 1 | 0 | 1 | 83 |
| 16:00 | 4 | 64 | 7 | 2 | 1 | 3 | 2 | 1 | 4 | 2 | 2 | 3 | 2 | 97 |
| 17:00 | 6 | 49 | 6 | 3 | 6 | 11 | 2 | 1 | 6 | 0 | 0 | 1 | 4 | 95 |
| 18:00 | 6 | 19 | 8 | 4 | 3 | 8 | 8 | 0 | 2 | 1 | 0 | 2 | 2 | 63 |
| 19:00 | 6 | 12 | 5 | 7 | 1 | 4 | 4 | 1 | 2 | 1 | 0 | 1 | 4 | 48 |
| 20:00 | 1 | 15 | 11 | 0 | 0 | 2 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 33 |
| 21:00 | 1 | 7 | 0 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 22:00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 23:00 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| $\begin{aligned} & \text { Day } \\ & \text { Total } \end{aligned}$ | 65 | 502 | 117 | 52 | 55 | 68 | 36 | 5 | 36 | 13 | 3 | 16 | 35 | 1003 |
| Percent | 6.5\% | 50.0\% | 11.7\% | 5.2\% | 5.5\% | 6.8\% | 3.6\% | 0.5\% | 3.6\% | 1.3\% | 0.3\% | 1.6\% | 3.5\% |  |
| AM Peak | 09:00 | 11:00 | 10:00 | 09:00 | 11:00 | 11:00 | 10:00 |  | 10:00 | 11:00 |  | 09:00 | 11:00 | 11:00 |
| Vol. | 9 | 62 | 19 | 5 | 7 | 5 | 4 |  | 5 | 4 |  | 2 | 4 | 101 |
| PM Peak | 15:00 | 16:00 | 12:00 | 14:00 | 15:00 | 17:00 | 18:00 | 12:00 | 17:00 | 16:00 | 16:00 | 14:00 | 13:00 | 16:00 |
| Vol. | 6 | 64 | 15 | 9 | 9 | 11 | 8 | 1 | 6 | 2 | 2 | 3 | 6 | 97 |
| Grand Total | 65 | 502 | 117 | 52 | 55 | 68 | 36 | 5 | 36 | 13 | 3 | 16 | 35 | 1003 |
| Percent | 6.5\% | 50.0\% | 11.7\% | 5.2\% | 5.5\% | 6.8\% | 3.6\% | 0.5\% | 3.6\% | 1.3\% | 0.3\% | 1.6\% | 3.5\% |  |

Produce Row east of Tucson - Nogales Hwy

| EB, WB Latitude: 0 ' 0.000 Undefined |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start |  | Cars \& | 2 Axle |  | 2 Axle | 3 Axle | 4 Axle | <5 Axle | 5 Axle | >6 Axle | <6 Axle | 6 Axle | >6 Axle |  |
| Time | Bikes | Tlirs | Long | Buses | 6 Tire | Single | Single | Double | Double | Double | Multi | Multi | Multi | Total |
| 2/4/15 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 01:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 02:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 03:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 04:00 | 1 | 4 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 9 |
| 05:00 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 4 |
| 06:00 | 2 | 11 | 0 | 0 | 3 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 18 |
| 07:00 | 2 | 61 | 16 | 2 | 1 | 0 | 0 | 1 | 4 | 0 | 0 | 0 | 0 | 87 |
| 08:00 | 5 | 86 | 18 | 0 | 4 | 1 | 3 | 1 | 2 | 3 | 0 | 0 | 0 | 123 |
| 09:00 | 14 | 129 | 31 | 5 | 7 | 3 | 2 | 2 | 5 | 0 | 0 | 2 | 4 | 204 |
| 10:00 | 8 | 108 | 33 | 6 | 13 | 5 | 5 | 2 | 9 | 4 | 0 | 2 | 4 | 199 |
| 11:00 | 11 | 111 | 22 | 6 | 13 | 9 | 1 | 1 | 11 | 5 | 0 | 2 | 6 | 198 |
| 12 PM | 6 | 79 | 22 | 7 | 11 | 14 | 1 | 1 | 7 | 1 | 0 | 2 | 7 | 158 |
| 13:00 | 9 | 45 | 14 | 13 | 11 | 8 | 4 | 1 | 12 | 1 | 0 | 0 | 10 | 128 |
| 14:00 | 8 | 53 | 12 | 14 | 9 | 9 | 6 | 2 | 5 | 2 | 0 | 3 | 5 | 128 |
| 15:00 | 7 | 66 | 17 | 9 | 13 | 6 | 6 | 0 | 14 | 2 | 2 | 0 | 3 | 145 |
| 16:00 | 9 | 97 | 10 | 5 | 4 | 6 | 5 | 4 | 9 | 6 | 5 | 5 | 3 | 168 |
| 17:00 | 9 | 85 | 12 | 5 | 8 | 14 | 7 | 2 | 9 | 2 | 0 | 1 | 5 | 159 |
| 18:00 | 10 | 32 | 11 | 5 | 6 | 9 | 9 | 1 | 7 | 3 | 0 | 2 | 4 | 99 |
| 19:00 | 6 | 13 | 6 | 9 | 1 | 6 | 4 | 1 | 5 | 2 | 0 | 1 | 4 | 58 |
| 20:00 | 3 | 17 | 11 | 0 | 0 | 3 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 40 |
| 21:00 | 2 | 9 | 0 | 0 | 2 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 16 |
| 22:00 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| 23:00 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 |
| $\begin{aligned} & \text { Day } \\ & \text { Total } \end{aligned}$ | 113 | 1009 | 239 | 86 | 108 | 94 | 54 | 20 | 106 | 34 | 7 | 20 | 56 | 1946 |
| Percent | 5.8\% | 51.8\% | 12.3\% | 4.4\% | 5.5\% | 4.8\% | 2.8\% | 1.0\% | 5.4\% | 1.7\% | 0.4\% | 1.0\% | 2.9\% |  |
| AM Peak | 09:00 | 09:00 | 10:00 | 10:00 | 10:00 | 11:00 | 10:00 | 09:00 | 11:00 | 11:00 |  | 09:00 | 11:00 | 09:00 |
| Vol. | 14 | 129 | 33 | 6 | 13 | 9 | 5 | 2 | 11 | 5 |  | 2 | 6 | 204 |
| PM Peak | 18:00 | 16:00 | 12:00 | 14:00 | 15:00 | 12:00 | 18:00 | 16:00 | 15:00 | 16:00 | 16:00 | 16:00 | 13:00 | 16:00 |
| Vol. | 10 | 97 | 22 | 14 | 13 | 14 | 9 | 4 | 14 | 6 | 5 | 5 | 10 | 168 |
| Grand Total | 113 | 1009 | 239 | 86 | 108 | 94 | 54 | 20 | 106 | 34 | 7 | 20 | 56 | 1946 |
| Percent | 5.8\% | 51.8\% | 12.3\% | 4.4\% | 5.5\% | 4.8\% | 2.8\% | 1.0\% | 5.4\% | 1.7\% | 0.4\% | 1.0\% | 2.9\% |  |


| EB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start |  | Cars \& | 2 Axle |  | $2 \text { Axle }$ | 3 Axle | 4 Axle | $<5 \text { Axle }$ | $5 \text { Axle }$ | >6 Axle | <6 Axle | 6 Axle | $>6 \text { Axle }$ |  |
| Time | Bikes | Tlrs | Long | Buses | 6 Tire | Single | Single | Double | Double | Double | Multi | Multi | Multi | Total |
| 2/4/15 | 0 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 01:00 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 02:00 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 03:00 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 04:00 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 |
| 05:00 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 06:00 | 0 | 35 | 11 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 47 |
| 07:00 | 0 | 104 | 13 | 1 | 0 | 5 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 126 |
| 08:00 | 0 | 86 | 24 | 0 | 0 | 2 | 1 | 4 | 0 | 0 | 0 | 0 | 0 | 117 |
| 09:00 | 0 | 75 | 22 | 0 | 2 | 2 | 1 | 0 | 1 | 0 | 0 | 1 | 0 | 104 |
| 10:00 | 0 | 106 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 107 |
| 11:00 | 1 | 102 | 16 | 1 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 123 |
| 12 PM | 0 | 125 | 46 | 0 | 5 | 0 | 0 | 3 | 2 | 1 | 0 | 0 | 2 | 184 |
| 13:00 | 0 | 54 | 17 | 1 | 0 | 2 | 0 | 1 | 1 | 1 | 0 | 0 | 0 | 77 |
| 14:00 | 1 | 121 | 52 | 1 | 0 | 2 | 1 | 2 | 3 | 0 | 0 | 0 | 0 | 183 |
| 15:00 | 0 | 139 | 45 | 1 | 1 | 3 | 0 | 0 | 5 | 0 | 0 | 0 | 1 | 195 |
| 16:00 | 0 | 216 | 40 | 0 | 1 | 2 | 6 | 4 | 6 | 2 | 0 | 1 | 0 | 278 |
| 17:00 | 0 | 168 | 37 | 0 | 3 | 1 | 0 | 1 | 2 | 1 | 1 | 0 | 1 | 215 |
| 18:00 | 0 | 120 | 31 | 0 | 1 | 3 | 1 | 3 | 4 | 0 | 0 | 0 | 0 | 163 |
| 19:00 | 0 | 94 | 14 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 109 |
| 20:00 | 0 | 57 | 12 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 72 |
| 21:00 | 0 | 37 | 16 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 53 |
| 22:00 | 0 | 23 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 32 |
| 23:00 | 0 | 12 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| Day Total | 2 | 1696 | 413 | 5 | 15 | 23 | 11 | 19 | 29 | 5 | 2 | 2 | 4 | 2226 |
| Percent | 0.1\% | 76.2\% | 18.6\% | 0.2\% | 0.7\% | 1.0\% | 0.5\% | 0.9\% | 1.3\% | 0.2\% | 0.1\% | 0.1\% | 0.2\% |  |
| AM Peak | 11:00 | 10:00 | 08:00 | 07:00 | 09:00 | 07:00 | 07:00 | 08:00 | 07:00 |  |  | 09:00 |  | 07:00 |
| Vol. | 1 | 106 | 24 | 1 | 2 | 5 | 1 | 4 | 2 |  |  | 1 |  | 126 |
| PM Peak | 14:00 | 16:00 | 14:00 | 13:00 | 12:00 | 15:00 | 16:00 | 16:00 | 16:00 | 16:00 | 17:00 | 16:00 | 12:00 | 16:00 |
| Vol. | 1 | 216 | 52 | 1 | 5 | 3 | 6 | 4 | 6 | 2 | 1 | 1 | 2 | 278 |
| Grand Total | 2 | 1696 | 413 | 5 | 15 | 23 | 11 | 19 | 29 | 5 | 2 | 2 | 4 | 2226 |
| Percent | 0.1\% | 76.2\% | 18.6\% | 0.2\% | 0.7\% | 1.0\% | 0.5\% | 0.9\% | 1.3\% | 0.2\% | 0.1\% | 0.1\% | 0.2\% |  |


| WB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start |  | Cars \& | 2 Axle |  | 2 Axle | 3 Axle | 4 Axle | <5 Axle | 5 Axle | >6 Axle | <6 Axle | 6 Axle | >6 Axle |  |
| Time | Bikes | Tlrs | Long | Buses | 6 Tire | Single | Single | Double | Double | Double | Multi | Multi | Multi | Total |
| 2/4/15 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| 01:00 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 02:00 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 03:00 | 0 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 04:00 | 0 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 05:00 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 06:00 | 0 | 71 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 89 |
| 07:00 | 0 | 149 | 48 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 200 |
| 08:00 | 0 | 90 | 38 | 0 | 1 | 1 | 0 | 0 | 3 | 0 | 0 | 0 | 1 | 134 |
| 09:00 | 0 | 107 | 34 | 1 | 1 | 2 | 0 | 1 | 1 | 0 | 0 | 0 | 1 | 148 |
| 10:00 | 4 | 102 | 13 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 121 |
| 11:00 | 3 | 87 | 28 | 2 | 3 | 0 | 1 | 0 | 4 | 0 | 0 | 0 | 0 | 128 |
| 12 PM | 5 | 128 | 56 | 1 | 5 | 3 | 2 | 6 | 3 | 1 | 0 | 1 | 1 | 212 |
| 13:00 | 10 | 117 | 40 | 1 | 1 | 2 | 1 | 1 | 4 | 0 | 0 | 0 | 2 | 179 |
| 14:00 | 0 | 102 | 47 | 1 | 1 | 0 | 0 | 2 | 2 | 0 | 0 | 0 | 0 | 155 |
| 15:00 | 0 | 111 | 58 | 1 | 0 | 2 | 0 | 1 | 2 | 0 | 0 | 1 | 3 | 179 |
| 16:00 | 3 | 127 | 44 | 1 | 3 | 1 | 4 | 8 | 3 | 1 | 1 | 1 | 2 | 199 |
| 17:00 | 0 | 159 | 50 | 0 | 2 | 1 | 1 | 1 | 1 | 2 | 0 | 1 | 0 | 218 |
| 18:00 | 0 | 93 | 26 | 0 | 0 | 0 | 0 | 1 | 5 | 0 | 0 | 0 | 1 | 126 |
| 19:00 | 0 | 49 | 19 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 70 |
| 20:00 | 0 | 44 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 53 |
| 21:00 | 0 | 20 | 8 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 30 |
| 22:00 | 0 | 11 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 15 |
| 23:00 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 |
| $\begin{aligned} & \text { Day } \\ & \text { Total } \end{aligned}$ | 25 | 1600 | 543 | 8 | 19 | 12 | 10 | 22 | 34 | 4 | 1 | 4 | 11 | 2293 |
| Percent | 1.1\% | 69.8\% | 23.7\% | 0.3\% | 0.8\% | 0.5\% | 0.4\% | 1.0\% | 1.5\% | 0.2\% | 0.0\% | 0.2\% | 0.5\% |  |
| AM Peak | 10:00 | 07:00 | 07:00 | 11:00 | 11:00 | 09:00 | 07:00 | 09:00 | 11:00 |  |  |  | 08:00 | 07:00 |
| Vol. | 4 | 149 | 48 | 2 | 3 | 2 | 1 | 1 | 4 |  |  |  | 1 | 200 |
| PM Peak | 13:00 | 17:00 | 15:00 | 12:00 | 12:00 | 12:00 | 16:00 | 16:00 | 18:00 | 17:00 | 16:00 | 12:00 | 15:00 | 17:00 |
| Vol. | 10 | 159 | 58 | 1 | 5 | 3 | 4 | 8 | 5 | 2 | 1 | 1 | 3 | 218 |
| Grand Total | 25 | 1600 | 543 | 8 | 19 | 12 | 10 | 22 | 34 | 4 | 1 | 4 | 11 | 2293 |
| Percent | 1.1\% | 69.8\% | 23.7\% | 0.3\% | 0.8\% | 0.5\% | 0.4\% | 1.0\% | 1.5\% | 0.2\% | 0.0\% | 0.2\% | 0.5\% |  |


| EB, WB |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start |  | Cars \& | 2 Axle |  | 2 Axle | 3 Axle | 4 Axle | <5 Axle | 5 Axle | >6 Axle | <6 Axle | 6 Axle | >6 Axle |  |
| Time | Bikes | Tlrs | Long | Buses | 6 Tire | Single | Single | Double | Double | Double | Multi | Multi | Multi | Total |
| 2/4/15 | 0 | 9 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 |
| 01:00 | 0 | 5 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 02:00 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 |
| 03:00 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 |
| 04:00 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 |
| 05:00 | 0 | 15 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| 06:00 | 0 | 106 | 29 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 136 |
| 07:00 | 0 | 253 | 61 | 1 | 1 | 5 | 2 | 0 | 3 | 0 | 0 | 0 | 0 | 326 |
| 08:00 | 0 | 176 | 62 | 0 | 1 | 3 | 1 | 4 | 3 | 0 | 0 | 0 | 1 | 251 |
| 09:00 | 0 | 182 | 56 | 1 | 3 | 4 | 1 | 1 | 2 | 0 | 0 | 1 | 1 | 252 |
| 10:00 | 4 | 208 | 14 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 228 |
| 11:00 | 4 | 189 | 44 | 3 | 4 | 1 | 1 | 1 | 4 | 0 | 0 | 0 | 0 | 251 |
| 12 PM | 5 | 253 | 102 | 1 | 10 | 3 | 2 | 9 | 5 | 2 | 0 | 1 | 3 | 396 |
| 13:00 | 10 | 171 | 57 | 2 | 1 | 4 | 1 | 2 | 5 | 1 | 0 | 0 | 2 | 256 |
| 14:00 | 1 | 223 | 99 | 2 | 1 | 2 | 1 | 4 | 5 | 0 | 0 | 0 | 0 | 338 |
| 15:00 | 0 | 250 | 103 | 2 | 1 | 5 | 0 | 1 | 7 | 0 | 0 | 1 | 4 | 374 |
| 16:00 | 3 | 343 | 84 | 1 | 4 | 3 | 10 | 12 | 9 | 3 | 1 | 2 | 2 | 477 |
| 17:00 | 0 | 327 | 87 | 0 | 5 | 2 | 1 | 2 | 3 | 3 | 1 | 1 | 1 | 433 |
| 18:00 | 0 | 213 | 57 | 0 | 1 | 3 | 1 | 4 | 9 | 0 | 0 | 0 | 1 | 289 |
| 19:00 | 0 | 143 | 33 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 179 |
| 20:00 | 0 | 101 | 21 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 125 |
| 21:00 | 0 | 57 | 24 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 0 | 0 | 83 |
| 22:00 | 0 | 34 | 12 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 47 |
| 23:00 | 0 | 18 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 20 |
| $\begin{aligned} & \text { Day } \\ & \text { Total } \end{aligned}$ | 27 | 3296 | 956 | 13 | 34 | 35 | 21 | 41 | 63 | 9 | 3 | 6 | 15 | 4519 |
| Percent | 0.6\% | 72.9\% | 21.2\% | 0.3\% | 0.8\% | 0.8\% | 0.5\% | 0.9\% | 1.4\% | 0.2\% | 0.1\% | 0.1\% | 0.3\% |  |
| AM Peak | 10:00 | 07:00 | 08:00 | 11:00 | 11:00 | 07:00 | 07:00 | 08:00 | 11:00 |  |  | 09:00 | 08:00 | 07:00 |
| Vol. | 4 | 253 | 62 | 3 | 4 | 5 | 2 | 4 | 4 |  |  | 1 | 1 | 326 |
| PM Peak | 13:00 | 16:00 | 15:00 | 13:00 | 12:00 | 15:00 | 16:00 | 16:00 | 16:00 | 16:00 | 16:00 | 16:00 | 15:00 | 16:00 |
| Vol. | 10 | 343 | 103 | 2 | 10 | 5 | 10 | 12 | 9 | 3 | 1 | 2 | 4 | 477 |
| Grand Total | 27 | 3296 | 956 | 13 | 34 | 35 | 21 | 41 | 63 | 9 | 3 | 6 | 15 | 4519 |
| Percent | 0.6\% | 72.9\% | 21.2\% | 0.3\% | 0.8\% | 0.8\% | 0.5\% | 0.9\% | 1.4\% | 0.2\% | 0.1\% | 0.1\% | 0.3\% |  |

Appendix B - Stakeholder Interview Summary

## Kimley»)Horn

# Nogales - Constraints Analysis at Three (3) Bridges 

KHA Job \# 098036004

## Stakeholder Interviews Summary

3/6/2015

Stakeholder interviews were conducted on March 6 ${ }^{\text {th }}, 2015$ with members of the Fresh Produce Association of the Americas (FPAA).

Meetings were conducted at individual offices and at the FPAA building. Representatives from the following were interviewed:

- Pacific Brokerage
- City of Nogales (Land Development Department)
- J-C Distributing, Inc.
- Wholesome Family Farms
- Wilson Produce, LLC
- Harvey Trucking
- Fresh Produce of the Americas


## Summary

- General information regarding the port of entry (POE) was discussed. As of now, 1800 trucks per day come into Nogales, AZ from Mexico. With POE expansions, the goal is to double the inflow to approximately 3600 trucks per day. 10 years is the anticipated target for doubling the inflow of trucks.
- The typical rule-of-thumb ratio for American trucks vs. Mexican trucks is 2:1. However, other FPAA members mentioned the ratio may vary by product. Thus, increasing the number of American trucks for each Mexican truck. It was mentioned that 1 Mexican truck can generate 5-6 American trucks.
- The typical trend for American trucks is to have mixed loads or loads that involve less than the truckload. "Straight" loads are uncommon due to the demand for the fresh produce. Thus, requiring more American trucks for every Mexican truck to come into Nogales.
- It is common for Mexican trucks to pay the overweight fees (\$75) when coming into Nogales.


## Kimley»Horn

- It was also mentioned that along Calle Sonora, an increase in larger (18-wheel) trucks is occurring that are creating issues within the existing roadway geometries at Calle Sonora \& Smokey Lane. Generated by Delta Fresh Sales, LLC
- Anticipated constraints, according to the City of Nogales Land Development Department includes the railroad right-of-way.
- It was discussed that some of the existing warehouses have plans to expand their facilities in the area. Areas are zoned for industrial use, including land owned by Larry Harvey and J-C Distributing. Some of the immediate plans include:
- 110,000 SF J-C Distributing Warehouse within the vicinity of Produce Row
- 70,000 SF Warehouse which would include 4-5 cold rooms. Also, within the vicinity of Produce Row.
- Potential 130 acres of residential development off of Gold Hill Road towards the east. Unknown number of units or lot size at this time. However, the potential for increased residential traffic at Gold Hill Road \& Grand Avenue would increase significantly.
- Approximately, Wilson Produce, LLC can see up to 300 trucks per day. The facility has recently expanded, the trucks per day may be even higher.
- There was definitely a consensus that wider bridges are necessary with existing traffic conditions and essential as truck traffic increases. A multiple lane bridge is desired. Existing turn radii at the 3 intersections do not accommodate the standard size trucks. The majority of the congestion is caused by turning trucks.
- According to the FPAA members, peak seasons vary for different warehouses. Thus, depending on the produce. Typical peak occurs during January - May. For Wholesum Family Produce, peak is typically year round.
- Last year's growth was $17 \%$ which is not normal. Typical average growth rate per year is around 6-7\% per year.
- Signal at Gold Hill Road only allows for 1 truck to go through the intersection which has been some contributing factors for some collisions.
- The railroad crossing was cited as an issue as collisions involving trucks and trains is fairly common.
- An estimate of 5-7 trains per day cross through the area. It can take as much as 20 minutes for a train to clear an intersection, creating severe queues east of the railroad tracks.


## Appendix C - Synchro Output Files

| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  |  | $\$$ |  |  | * |  |
| Volume (veh/h) | 31 | 988 | 50 | 25 | 590 | 29 | 51 | 1 | 71 | 29 | 0 | 41 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1509 | 1717 | 1750 | 1750 | 1701 | 1750 | 1750 | 1740 | 1750 | 1750 | 1700 | 1750 |
| Adj Flow Rate, veh/h | 42 | 1353 | 68 | 30 | 711 | 35 | 64 | 1 | 89 | 43 | 0 | 60 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Peak Hour Factor | 0.73 | 0.73 | 0.73 | 0.83 | 0.83 | 0.83 | 0.80 | 0.80 | 0.80 | 0.68 | 0.68 | 0.68 |
| Percent Heavy Veh, \% | 16 | 2 | 2 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cap, veh/h | 390 | 1953 | 98 | 215 | 1937 | 95 | 205 | 28 | 224 | 206 | 24 | 224 |
| Arrive On Green | 0.62 | 0.62 | 0.62 | 0.62 | 0.62 | 0.62 | 0.27 | 0.27 | 0.27 | 0.27 | 0.00 | 0.27 |
| Sat Flow, veh/h | 577 | 3162 | 159 | 353 | 3136 | 154 | 498 | 101 | 820 | 499 | 89 | 822 |
| Grp Volume(v), veh/h | 42 | 697 | 724 | 30 | 366 | 380 | 154 | 0 | 0 | 103 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 577 | 1631 | 1689 | 353 | 1616 | 1674 | 1419 | 0 | 0 | 1410 | 0 | 0 |
| Q Serve(g_s), s | 2.8 | 20.9 | 21.0 | 4.5 | 8.2 | 8.2 | 2.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 11.1 | 20.9 | 21.0 | 25.6 | 8.2 | 8.2 | 6.0 | 0.0 | 0.0 | 3.7 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.09 | 1.00 |  | 0.09 | 0.42 |  | 0.58 | 0.42 |  | 0.58 |
| Lane Grp Cap(c), veh/h | 390 | 1008 | 1044 | 215 | 998 | 1034 | 457 | 0 | 0 | 455 | 0 | 0 |
| V/C Ratio(X) | 0.11 | 0.69 | 0.69 | 0.14 | 0.37 | 0.37 | 0.34 | 0.00 | 0.00 | 0.23 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 443 | 1158 | 1199 | 248 | 1147 | 1188 | 457 | 0 | 0 | 455 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 9.7 | 9.3 | 9.4 | 17.9 | 6.9 | 6.9 | 21.5 | 0.0 | 0.0 | 20.7 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.1 | 1.5 | 1.5 | 0.3 | 0.2 | 0.2 | 2.0 | 0.0 | 0.0 | 0.3 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.5 | 9.7 | 10.1 | 0.5 | 3.6 | 3.8 | 2.8 | 0.0 | 0.0 | 1.6 | 0.0 | 0.0 |
| LnGrp Delay(d),s/veh | 9.8 | 10.8 | 10.8 | 18.2 | 7.1 | 7.1 | 23.5 | 0.0 | 0.0 | 21.0 | 0.0 | 0.0 |
| LnGrp LOS | A | B | B | B | A | A | C |  |  | C |  |  |
| Approach Vol, veh/h |  | 1463 |  |  | 776 |  |  | 154 |  |  | 103 |  |
| Approach Delay, s/veh |  | 10.8 |  |  | 7.6 |  |  | 23.5 |  |  | 21.0 |  |
| Approach LOS |  | B |  |  | A |  |  | C |  |  | C |  |


| Timer | 1 | 2 | 3 | 4 | 5 | 6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 性 |  | ${ }^{7}$ | 中 ${ }^{\text {c }}$ |  | ${ }^{7}$ | $\hat{F}$ |  |  | \$ |  |
| Volume (veh/h) | 26 | 840 | 221 | 22 | 476 | 27 | 155 | 3 | 55 | 7 | 0 | 7 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial $Q(Q b)$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1522 | 1733 | 1750 | 1750 | 1685 | 1750 | 1750 | 1717 | 1750 | 1750 | 1362 | 1750 |
| Adj Flow Rate, veh/h | 34 | 1091 | 287 | 23 | 506 | 29 | 258 | 5 | 92 | 11 | 0 | 11 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 0 | 1 | 0 |
| Peak Hour Factor | 0.77 | 0.77 | 0.77 | 0.94 | 0.94 | 0.94 | 0.60 | 0.60 | 0.60 | 0.62 | 0.62 | 0.62 |
| Percent Heavy Veh, \% | 15 | 1 | 1 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cap, veh/h | 456 | 1260 | 329 | 236 | 1501 | 86 | 490 | 22 | 408 | 194 | 16 | 142 |
| Arrive On Green | 0.06 | 0.49 | 0.49 | 0.06 | 0.49 | 0.49 | 0.29 | 0.29 | 0.29 | 0.29 | 0.00 | 0.29 |
| Sat Flow, veh/h | 1449 | 2585 | 675 | 1667 | 3078 | 176 | 1313 | 76 | 1395 | 432 | 53 | 485 |
| Grp Volume(v), veh/h | 34 | 692 | 686 | 23 | 263 | 272 | 258 | 0 | 97 | 22 | 0 | 0 |
| Grp Sat Flow(s),veh/h/n | 1449 | 1646 | 1614 | 1667 | 1601 | 1654 | 1313 | 0 | 1471 | 970 | 0 | 0 |
| Q Serve(g_s), s | 0.9 | 29.7 | 30.3 | 0.5 | 8.0 | 8.1 | 8.6 | 0.0 | 4.0 | 0.0 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 0.9 | 29.7 | 30.3 | 0.5 | 8.0 | 8.1 | 12.7 | 0.0 | 4.0 | 4.0 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.42 | 1.00 |  | 0.11 | 1.00 |  | 0.95 | 0.50 |  | 0.50 |
| Lane Grp Cap(c), veh/h | 456 | 802 | 787 | 236 | 780 | 806 | 490 | 0 | 430 | 351 | 0 | 0 |
| V/C Ratio(X) | 0.07 | 0.86 | 0.87 | 0.10 | 0.34 | 0.34 | 0.53 | 0.00 | 0.23 | 0.06 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 456 | 802 | 787 | 236 | 780 | 806 | 490 | 0 | 430 | 351 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 8.7 | 18.1 | 18.3 | 14.3 | 12.6 | 12.6 | 24.2 | 0.0 | 21.4 | 20.4 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.3 | 11.8 | 12.8 | 0.8 | 1.2 | 1.1 | 4.0 | 0.0 | 1.2 | 0.3 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.4 | 15.9 | 16.1 | 0.3 | 3.8 | 3.9 | 5.5 | 0.0 | 1.8 | 0.4 | 0.0 | 0.0 |
| LnGrp Delay(d),s/veh | 9.0 | 29.9 | 31.1 | 15.1 | 13.7 | 13.7 | 28.3 | 0.0 | 22.6 | 20.7 | 0.0 | 0.0 |
| LnGrp LOS | A | C | c | B | B | B | C |  | C | C |  |  |
| Approach Vol, veh/h |  | 1412 |  |  | 558 |  |  | 355 |  |  | 22 |  |
| Approach Delay, s/veh |  | 30.0 |  |  | 13.8 |  |  | 26.7 |  |  | 20.7 |  |
| Approach LOS |  | C |  |  | B |  |  | C |  |  | C |  |


| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Assigned Phs | 2 | 3 | 4 | 6 | 7 | 8 |  |  |
| Phs Duration (G+Y+Rc), s | 27.4 | 9.6 | 43.0 |  | 27.4 | 9.6 | 43.0 |  |
| Change Period (Y+Rc), s | 4.0 | 4.5 | 4.0 | 4.0 | 4.5 | 4.0 |  |  |
| Max Green Setting (Gmax), s | 23.4 | 5.1 | 39.0 | 23.4 | 5.1 | 39.0 |  |  |
| Max Q Clear Time (g_c+11), s | 14.7 | 2.5 | 32.3 | 6.0 | 2.9 | 10.1 |  |  |
| Green Ext Time (p_c), s | 1.0 | 0.0 | 5.4 | 1.4 | 0.0 | 16.8 |  |  |

Intersection Summary
HCM 2010 Ctrl Delay
25.5

HCM 2010 LOS
C

|  | 3 | $\rightarrow$ | $\geqslant$ | 7 |  | 4 | $4$ | $\dagger$ | $p$ |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 4 | 「 |  | \＆ |  | ${ }^{*} 1$ | 中 ${ }^{\text {a }}$ |  | ＊ | 中4 | 「 |
| Volume（veh／h） | 160 | 61 | 190 | 52 | 111 | 36 | 208 | 365 | 28 | 45 | 523 | 224 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow，veh／h／ln | 1620 | 1636 | 1716 | 1750 | 1725 | 1750 | 1699 | 1725 | 1750 | 1606 | 1750 | 1667 |
| Adj Flow Rate，veh／h | 208 | 79 | 247 | 87 | 185 | 60 | 242 | 424 | 33 | 55 | 638 | 273 |
| Adj No．of Lanes | 2 | 1 | 1 | 0 | 1 | 0 | 2 | 2 | 0 | 1 | 2 | 1 |
| Peak Hour Factor | 0.77 | 0.77 | 0.77 | 0.60 | 0.60 | 0.60 | 0.86 | 0.86 | 0.86 | 0.82 | 0.82 | 0.82 |
| Percent Heavy Veh，\％ | 8 | 7 | 2 | 0 | 0 | 0 | 3 | 1 | 1 | 9 | 0 | 5 |
| Cap，veh／h | 561 | 307 | 273 | 99 | 210 | 68 | 306 | 1132 | 88 | 67 | 1028 | 438 |
| Arrive On Green | 0.19 | 0.19 | 0.19 | 0.23 | 0.23 | 0.23 | 0.10 | 0.37 | 0.37 | 0.04 | 0.31 | 0.31 |
| Sat Flow，veh／h | 2994 | 1636 | 1458 | 433 | 920 | 298 | 3139 | 3083 | 239 | 1529 | 3325 | 1417 |
| Grp Volume（v），veh／h | 208 | 79 | 247 | 332 | 0 | 0 | 242 | 225 | 232 | 55 | 638 | 273 |
| Grp Sat Flow（s），veh／h／ln | 1497 | 1636 | 1458 | 1651 | 0 | 0 | 1570 | 1639 | 1683 | 1529 | 1663 | 1417 |
| Q Serve（g＿s），s | 6.7 | 4.5 | 18.2 | 21.3 | 0.0 | 0.0 | 8.3 | 11.0 | 11.1 | 3.9 | 18.0 | 18.1 |
| Cycle Q Clear（g＿c），s | 6.7 | 4.5 | 18.2 | 21.3 | 0.0 | 0.0 | 8.3 | 11.0 | 11.1 | 3.9 | 18.0 | 18.1 |
| Prop In Lane | 1.00 |  | 1.00 | 0.26 |  | 0.18 | 1.00 |  | 0.14 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 561 | 307 | 273 | 377 | 0 | 0 | 306 | 602 | 618 | 67 | 1028 | 438 |
| V／C Ratio（X） | 0.37 | 0.26 | 0.90 | 0.88 | 0.00 | 0.00 | 0.79 | 0.37 | 0.38 | 0.82 | 0.62 | 0.62 |
| Avail Cap（c＿a），veh／h | 595 | 325 | 290 | 570 | 0 | 0 | 478 | 602 | 618 | 153 | 1033 | 440 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 38.9 | 38.1 | 43.6 | 40.9 | 0.0 | 0.0 | 48.4 | 25.5 | 25.5 | 52.0 | 32.4 | 32.4 |
| Incr Delay（d2），s／veh | 0.4 | 0.4 | 28.6 | 10.3 | 0.0 | 0.0 | 4.8 | 1.8 | 1.7 | 20.5 | 1.1 | 2.7 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 2.8 | 2.1 | 9.5 | 10.8 | 0.0 | 0.0 | 3.8 | 5.3 | 5.5 | 2.0 | 8.4 | 7.4 |
| LnGrp Delay（d），s／veh | 39.3 | 38.5 | 72.2 | 51.2 | 0.0 | 0.0 | 53.2 | 27.2 | 27.2 | 72.6 | 33.5 | 35.1 |
| LnGrp LOS | D | D | E | D |  |  | D | C | C | E | C | D |
| Approach Vol，veh／h |  | 534 |  |  | 332 |  |  | 699 |  |  | 966 |  |
| Approach Delay，s／veh |  | 54.4 |  |  | 51.2 |  |  | 36.2 |  |  | 36.2 |  |
| Approach LOS |  | D |  |  | D |  |  | D |  |  | D |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R c$ ），$s$ | 9.8 | 45.3 |  | 25.1 | 16.2 | 38.9 |  | 29.5 |  |  |  |  |
| Change Period（Y＋Rc），s | 5.0 | 5.0 |  | 4.5 | 5.5 | 5.0 |  | 4.5 |  |  |  |  |
| Max Green Setting（Gmax），s | 11.0 | 40.3 |  | 21.8 | 16.7 | 34.1 |  | 37.9 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 5.9 | 13.1 |  | 20.2 | 10.3 | 20.1 |  | 23.3 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 9.5 |  | 0.4 | 0.4 | 6.9 |  | 1.7 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 42.0 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | D |  |  |  |  |  |  |  |  |  |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 郎 |  | ${ }^{7}$ | 郎 |  |  | $\leqslant$ |  |  | ¢ |  |
| Volume (veh/h) | 42 | 628 | 58 | 56 | 801 | 52 | 76 | 7 | 56 | 70 | 8 | 63 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1496 | 1645 | 1750 | 1750 | 1644 | 1750 | 1750 | 1743 | 1750 | 1750 | 1538 | 1750 |
| Adj Flow Rate, veh/h | 43 | 641 | 59 | 58 | 826 | 54 | 85 | 8 | 63 | 74 | 8 | 66 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 0 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.97 | 0.97 | 0.97 | 0.89 | 0.89 | 0.89 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, \% | 17 | 7 | 7 | 0 | 6 | 6 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cap, veh/h | 251 | 1403 | 129 | 342 | 1443 | 94 | 364 | 50 | 225 | 305 | 48 | 220 |
| Arrive On Green | 0.48 | 0.48 | 0.48 | 0.48 | 0.48 | 0.48 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 | 0.40 |
| Sat Flow, veh/h | 504 | 2894 | 266 | 698 | 2977 | 195 | 709 | 127 | 566 | 568 | 120 | 553 |
| Grp Volume(v), veh/h | 43 | 346 | 354 | 58 | 433 | 447 | 156 | 0 | 0 | 148 | 0 | 0 |
| Grp Sat Flow(s),veh/h/ln | 504 | 1562 | 1598 | 698 | 1562 | 1610 | 1403 | 0 | 0 | 1241 | 0 | 0 |
| Q Serve(g_s), s | 4.5 | 9.9 | 10.0 | 4.1 | 13.4 | 13.4 | 0.0 | 0.0 | 0.0 | 0.5 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 18.0 | 9.9 | 10.0 | 14.0 | 13.4 | 13.4 | 4.2 | 0.0 | 0.0 | 4.7 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.17 | 1.00 |  | 0.12 | 0.54 |  | 0.40 | 0.50 |  | 0.45 |
| Lane Grp Cap(c), veh/h | 251 | 757 | 774 | 342 | 757 | 780 | 639 | 0 | 0 | 573 | 0 | 0 |
| V/C Ratio(X) | 0.17 | 0.46 | 0.46 | 0.17 | 0.57 | 0.57 | 0.24 | 0.00 | 0.00 | 0.26 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 340 | 1035 | 1058 | 466 | 1035 | 1066 | 639 | 0 | 0 | 573 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 18.9 | 11.6 | 11.6 | 16.2 | 12.5 | 12.5 | 13.6 | 0.0 | 0.0 | 13.7 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.3 | 0.4 | 0.4 | 0.2 | 0.7 | 0.7 | 0.9 | 0.0 | 0.0 | 0.2 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/In | 0.6 | 4.3 | 4.4 | 0.8 | 5.9 | 6.1 | 2.1 | 0.0 | 0.0 | 1.9 | 0.0 | 0.0 |
| LnGrp Delay(d),s/veh | 19.2 | 12.0 | 12.0 | 16.5 | 13.2 | 13.1 | 14.5 | 0.0 | 0.0 | 14.0 | 0.0 | 0.0 |
| LnGrp LOS | B | B | B | B | B | B | B |  |  | B |  |  |
| Approach Vol, veh/h |  | 743 |  |  | 938 |  |  | 156 |  |  | 148 |  |
| Approach Delay, s/veh |  | 12.4 |  |  | 13.4 |  |  | 14.5 |  |  | 14.0 |  |
| Approach LOS |  | B |  |  | B |  |  | B |  |  | B |  |


| Timer | 1 | 2 | 3 | 4 | 5 | 6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{*}$ | 中 ${ }^{\text {W }}$ |  | ${ }^{7}$ | $\uparrow$ |  |  | \& |  |
| Volume (veh/h) | 33 | 596 | 154 | 50 | 740 | 33 | 161 | 5 | 49 | 48 | 8 | 62 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1378 | 1661 | 1750 | 1562 | 1619 | 1750 | 1683 | 1458 | 1750 | 1750 | 1378 | 1750 |
| Adj Flow Rate, veh/h | 35 | 627 | 162 | 59 | 871 | 39 | 196 | 6 | 60 | 70 | 12 | 90 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 0 | 1 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.85 | 0.85 | 0.85 | 0.82 | 0.82 | 0.82 | 0.69 | 0.69 | 0.69 |
| Percent Heavy Veh, \% | 27 | 6 | 6 | 12 | 6 | 6 | 4 | 20 | 20 | 0 | 0 | 0 |
| Cap, veh/h | 216 | 962 | 248 | 275 | 1201 | 54 | 540 | 45 | 446 | 227 | 51 | 228 |
| Arrive On Green | 0.03 | 0.39 | 0.39 | 0.05 | 0.40 | 0.40 | 0.39 | 0.39 | 0.39 | 0.39 | 0.39 | 0.39 |
| Sat Flow, veh/h | 1312 | 2484 | 641 | 1488 | 2999 | 134 | 1163 | 114 | 1142 | 400 | 131 | 583 |
| Grp Volume(v), veh/h | 35 | 398 | 391 | 59 | 447 | 463 | 196 | 0 | 66 | 172 | 0 | 0 |
| Grp Sat Flow(s), veh/h/ln | 1312 | 1578 | 1548 | 1488 | 1538 | 1595 | 1163 | 0 | 1257 | 1114 | 0 | 0 |
| Q Serve(g_s), s | 1.1 | 14.8 | 14.9 | 1.7 | 17.6 | 17.6 | 2.3 | 0.0 | 2.4 | 4.7 | 0.0 | 0.0 |
| Cycle Q Clear(g_c), s | 1.1 | 14.8 | 14.9 | 1.7 | 17.6 | 17.6 | 10.0 | 0.0 | 2.4 | 7.6 | 0.0 | 0.0 |
| Prop In Lane | 1.00 |  | 0.41 | 1.00 |  | 0.08 | 1.00 |  | 0.91 | 0.41 |  | 0.52 |
| Lane Grp Cap(c), veh/h | 216 | 611 | 599 | 275 | 616 | 639 | 540 | 0 | 491 | 506 | 0 | 0 |
| V/C Ratio(X) | 0.16 | 0.65 | 0.65 | 0.21 | 0.73 | 0.73 | 0.36 | 0.00 | 0.13 | 0.34 | 0.00 | 0.00 |
| Avail Cap(c_a), veh/h | 271 | 717 | 703 | 347 | 729 | 756 | 540 | 0 | 491 | 506 | 0 | 0 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(I) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 0.00 |
| Uniform Delay (d), s/veh | 14.4 | 18.0 | 18.0 | 13.6 | 18.2 | 18.2 | 16.5 | 0.0 | 14.1 | 15.6 | 0.0 | 0.0 |
| Incr Delay (d2), s/veh | 0.3 | 1.6 | 1.7 | 0.4 | 3.0 | 2.9 | 1.9 | 0.0 | 0.6 | 0.4 | 0.0 | 0.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.4 | 6.7 | 6.6 | 0.7 | 8.0 | 8.2 | 3.2 | 0.0 | 0.9 | 2.5 | 0.0 | 0.0 |
| LnGrp Delay(d),s/veh | 14.7 | 19.7 | 19.7 | 14.0 | 21.1 | 21.0 | 18.3 | 0.0 | 14.6 | 16.0 | 0.0 | 0.0 |
| LnGrp LOS | B | B | B | B | C | C | B |  | B | B |  |  |
| Approach Vol, veh/h |  | 824 |  |  | 969 |  |  | 262 |  |  | 172 |  |
| Approach Delay, s/veh |  | 19.5 |  |  | 20.7 |  |  | 17.4 |  |  | 16.0 |  |
| Approach LOS |  | B |  |  | C |  |  | B |  |  | B |  |


| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Assigned Phs | 2 | 3 | 4 | 6 | 7 | 8 |  |
| Phs Duration (G+Y+Rc), s | 32.0 | 8.0 | 31.8 |  | 32.0 | 7.0 | 32.7 |
| Change Period (Y+Rc), s | 4.0 | 4.5 | 4.0 | 4.0 | 4.5 | 4.0 |  |
| Max Green Setting (Gmax), s | 28.0 | 6.9 | 32.6 | 28.0 | 5.5 | 34.0 |  |
| Max Q Clear Time (g_c+I1), s | 12.0 | 3.7 | 16.9 | 9.6 | 3.1 | 19.6 |  |
| Green Ext Time (p_C), s | 2.0 | 0.0 | 9.7 | 2.1 | 0.0 | 9.1 |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  | 19.5 |  |  |  |  |  |
| HCM 2010 LOS | B |  |  |  |  |  |  |


|  | ＊ |  | $\stackrel{\square}{7}$ | 7 |  | 4 |  | $\dagger$ | 7 | $t$ | $\ddagger$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 4 | 4 | 「 |  | 4 |  | 4 | 㻢 |  | ${ }^{1}$ | 44 | 「 |
| Volume（veh／h） | 396 | 123 | 267 | 42 | 99 | 78 | 345 | 532 | 46 | 76 | 501 | 205 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow，veh／h／ln | 1549 | 1636 | 1716 | 1750 | 1625 | 1750 | 1699 | 1734 | 1750 | 1535 | 1699 | 1496 |
| Adj Flow Rate，veh／h | 455 | 141 | 307 | 56 | 132 | 104 | 416 | 641 | 55 | 84 | 557 | 228 |
| Adj No．of Lanes | 2 | 1 | 1 | 0 | 1 | 0 | 2 | 2 | 0 | 1 | 2 | 1 |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.75 | 0.75 | 0.75 | 0.83 | 0.83 | 0.83 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh，\％ | 13 | 7 | 2 | 6 | 6 | 6 | 3 | 1 | 1 | 14 | 3 | 17 |
| Cap，veh／h | 581 | 332 | 296 | 70 | 165 | 130 | 542 | 975 | 84 | 135 | 753 | 296 |
| Arrive On Green | 0.20 | 0.20 | 0.20 | 0.24 | 0.24 | 0.24 | 0.17 | 0.32 | 0.32 | 0.09 | 0.23 | 0.23 |
| Sat Flow，veh／h | 2861 | 1636 | 1458 | 291 | 685 | 540 | 3139 | 3072 | 263 | 1462 | 3228 | 1271 |
| Grp Volume（v），veh／h | 455 | 141 | 307 | 292 | 0 | 0 | 416 | 343 | 353 | 84 | 557 | 228 |
| Grp Sat Flow（s），veh／h／ln | 1431 | 1636 | 1458 | 1515 | 0 | 0 | 1570 | 1647 | 1688 | 1462 | 1614 | 1271 |
| Q Serve（g＿s），s | 19.6 | 9.8 | 26.5 | 23.6 | 0.0 | 0.0 | 16.5 | 23.4 | 23.5 | 7.2 | 20.9 | 21.9 |
| Cycle Q Clear（g＿c），s | 19.6 | 9.8 | 26.5 | 23.6 | 0.0 | 0.0 | 16.5 | 23.4 | 23.5 | 7.2 | 20.9 | 21.9 |
| Prop In Lane | 1.00 |  | 1.00 | 0.19 |  | 0.36 | 1.00 |  | 0.16 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 581 | 332 | 296 | 366 | 0 | 0 | 542 | 523 | 536 | 135 | 753 | 296 |
| V／C Ratio（X） | 0.78 | 0.42 | 1.04 | 0.80 | 0.00 | 0.00 | 0.77 | 0.66 | 0.66 | 0.62 | 0.74 | 0.77 |
| Avail Cap（c＿a），veh／h | 581 | 332 | 296 | 366 | 0 | 0 | 542 | 523 | 536 | 135 | 753 | 296 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（l） | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 49.2 | 45.3 | 51.9 | 46.5 | 0.0 | 0.0 | 51.5 | 38.4 | 38.4 | 57.0 | 46.3 | 46.7 |
| Incr Delay（d2），s／veh | 10.1 | 3.9 | 61.9 | 16.4 | 0.0 | 0.0 | 10.0 | 6.3 | 6.2 | 19.9 | 6.5 | 17.3 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／In | 8.6 | 4.8 | 15.8 | 11.6 | 0.0 | 0.0 | 7.9 | 11.6 | 11.9 | 3.7 | 10.0 | 9.1 |
| LnGrp Delay（d），s／veh | 59.3 | 49.2 | 113.8 | 62.9 | 0.0 | 0.0 | 61.5 | 44.7 | 44.6 | 76.9 | 52.8 | 64.1 |
| LnGrp LOS | E | D | F | E |  |  | E | D | D | E | D | E |
| Approach Vol，veh／h |  | 903 |  |  | 292 |  |  | 1112 |  |  | 869 |  |
| Approach Delay，s／veh |  | 76.3 |  |  | 62.9 |  |  | 51.0 |  |  | 58.1 |  |
| Approach LOS |  | E |  |  | E |  |  | D |  |  | E |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs | 1 | 2 |  | 4 | 5 | 6 |  | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R \mathrm{c}$ ），$s$ | 17.0 | 46.4 |  | 31.0 | 28.0 | 35.4 |  | 36.0 |  |  |  |  |
| Change Period（Y＋Rc），s | 5.0 | 5.0 |  | 4.5 | 5.5 | 5.0 |  | 4.5 |  |  |  |  |
| Max Green Setting（Gmax），s | 12.0 | 41.4 |  | 26.5 | 22.5 | 30.4 |  | 31.5 |  |  |  |  |
| Max Q Clear Time（g＿c＋11），s | 9.2 | 25.5 |  | 28.5 | 18.5 | 23.9 |  | 25.6 |  |  |  |  |
| Green Ext Time（p＿c），s | 1.3 | 3.9 |  | 0.0 | 0.6 | 2.6 |  | 0.8 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 61.2 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | E |  |  |  |  |  |  |  |  |  |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{7}$ | 中 ${ }^{\text {W }}$ |  | ${ }^{7}$ | $\hat{\beta}$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Volume (veh/h) | 40 | 1284 | 65 | 33 | 767 | 38 | 58 | 1 | 81 | 62 | 0 | 85 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 0.90 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1552 | 1766 | 1800 | 1800 | 1750 | 1800 | 1800 | 1765 | 1800 | 1800 | 1698 | 1800 |
| Adj Flow Rate, veh/h | 55 | 1759 | 89 | 40 | 924 | 46 | 72 | 1 | 101 | 91 | 0 | 125 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 0.73 | 0.73 | 0.73 | 0.83 | 0.83 | 0.83 | 0.80 | 0.80 | 0.80 | 0.68 | 0.68 | 0.68 |
| Percent Heavy Veh, \% | 16 | 2 | 2 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 |
| Cap, veh/h | 65 | 1613 | 81 | 61 | 1656 | 82 | 316 | 3 | 284 | 345 | 0 | 291 |
| Arrive On Green | 0.04 | 0.52 | 0.52 | 0.04 | 0.51 | 0.51 | 0.05 | 0.19 | 0.19 | 0.06 | 0.00 | 0.20 |
| Sat Flow, veh/h | 1478 | 3086 | 155 | 1714 | 3224 | 160 | 1714 | 15 | 1488 | 1714 | 0 | 1443 |
| Grp Volume(v), veh/h | 55 | 951 | 897 | 40 | 477 | 493 | 72 | 0 | 102 | 91 | 0 | 125 |
| Grp Sat Flow(s), veh/h/ln | 1478 | 1678 | 1562 | 1714 | 1662 | 1722 | 1714 | 0 | 1502 | 1714 | 0 | 1443 |
| Q Serve(g_s), s | 3.3 | 46.0 | 46.0 | 2.0 | 17.2 | 17.2 | 2.9 | 0.0 | 5.2 | 3.7 | 0.0 | 6.7 |
| Cycle Q Clear(g_c), s | 3.3 | 46.0 | 46.0 | 2.0 | 17.2 | 17.2 | 2.9 | 0.0 | 5.2 | 3.7 | 0.0 | 6.7 |
| Prop In Lane | 1.00 |  | 0.10 | 1.00 |  | 0.09 | 1.00 |  | 0.99 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 65 | 877 | 817 | 61 | 854 | 885 | 316 | 0 | 287 | 345 | 0 | 291 |
| V/C Ratio(X) | 0.84 | 1.08 | 1.10 | 0.66 | 0.56 | 0.56 | 0.23 | 0.00 | 0.36 | 0.26 | 0.00 | 0.43 |
| Avail Cap(c_a), veh/h | 141 | 877 | 817 | 99 | 854 | 885 | 335 | 0 | 287 | 345 | 0 | 291 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(l) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 41.7 | 21.0 | 21.0 | 41.9 | 14.6 | 14.6 | 26.9 | 0.0 | 30.9 | 26.4 | 0.0 | 30.7 |
| Incr Delay (d2), s/veh | 23.5 | 55.7 | 62.1 | 11.5 | 0.8 | 0.8 | 0.4 | 0.0 | 3.4 | 0.4 | 0.0 | 1.0 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.8 | 34.8 | 33.8 | 1.1 | 8.0 | 8.3 | 1.4 | 0.0 | 2.4 | 1.8 | 0.0 | 2.7 |
| LnGrp Delay(d),s/veh | 65.3 | 76.7 | 83.1 | 53.4 | 15.4 | 15.4 | 27.2 | 0.0 | 34.3 | 26.8 | 0.0 | 31.7 |
| LnGrp LOS | E | F | F | D | B | B | C |  | C | C |  | C |
| Approach Vol, veh/h |  | 1903 |  |  | 1010 |  |  | 174 |  |  | 216 |  |
| Approach Delay, s/veh |  | 79.4 |  |  | 16.9 |  |  | 31.4 |  |  | 29.6 |  |
| Approach LOS |  | E |  |  | B |  |  | C |  |  | C |  |


| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration (G+Y+Rc), s | 9.6 | 20.8 | 7.6 | 50.0 | 8.6 | 21.7 | 8.4 | 49.2 |
| Change Period (Y+Rc), s | 4.5 | 4.0 | 4.5 | 4.0 | 4.5 | 4.0 | 4.5 | 4.0 |
| Max Green Setting (Gmax), s | 5.1 | 16.8 | 5.1 | 46.0 | 5.1 | 16.8 | 8.4 | 42.7 |
| Max Q Clear Time (g_c+11), s | 5.7 | 7.2 | 4.0 | 48.0 | 4.9 | 8.7 | 5.3 | 19.2 |
| Green Ext Time (p_c), s | 0.0 | 0.9 | 0.0 | 0.0 | 0.0 | 0.8 | 0.0 | 19.4 |


| Intersection Summary |  |
| :--- | ---: |
| HCM 2010 Ctrl Delay | 54.5 |
| HCM 2010 LOS | D |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | 个 ${ }_{\text {d }}$ |  | \% | 性 |  | * | $\hat{\beta}$ |  | * | $\hat{\beta}$ |  |
| Volume (veh/h) | 34 | 1092 | 287 | 29 | 619 | 35 | 202 | 4 | 72 | 8 | 0 | 11 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial $\mathrm{Q}(\mathrm{Qb})$, veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1522 | 1733 | 1750 | 1750 | 1685 | 1750 | 1750 | 1718 | 1750 | 1357 | 1067 | 1750 |
| Adj Flow Rate, veh/h | 44 | 1418 | 373 | 31 | 659 | 37 | 337 | 7 | 120 | 13 | 0 | 18 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 0.77 | 0.77 | 0.77 | 0.94 | 0.94 | 0.94 | 0.60 | 0.60 | 0.60 | 0.62 | 0.62 | 0.62 |
| Percent Heavy Veh, \% | 15 | 1 | 1 | 0 | 3 | 3 | 0 | 0 | 0 | 29 | 0 | 0 |
| Cap, veh/h | 390 | 1425 | 363 | 133 | 1668 | 94 | 427 | 23 | 388 | 275 | 0 | 253 |
| Arrive On Green | 0.04 | 0.55 | 0.55 | 0.03 | 0.54 | 0.54 | 0.28 | 0.28 | 0.28 | 0.28 | 0.00 | 0.28 |
| Sat Flow, veh/h | 1449 | 2599 | 663 | 1667 | 3083 | 173 | 1305 | 81 | 1391 | 916 | 0 | 907 |
| Grp Volume(v), veh/h | 44 | 882 | 909 | 31 | 342 | 354 | 337 | 0 | 127 | 13 | 0 | 18 |
| Grp Sat Flow(s),veh/h/n | 1449 | 1646 | 1616 | 1667 | 1601 | 1655 | 1305 | 0 | 1472 | 916 | 0 | 907 |
| Q Serve(g_s), s | 1.2 | 45.6 | 48.0 | 0.7 | 10.9 | 10.9 | 22.4 | 0.0 | 6.0 | 1.0 | 0.0 | 1.3 |
| Cycle Q Clear(g_c), s | 1.2 | 45.6 | 48.0 | 0.7 | 10.9 | 10.9 | 23.7 | 0.0 | 6.0 | 7.0 | 0.0 | 1.3 |
| Prop In Lane | 1.00 |  | 0.41 | 1.00 |  | 0.10 | 1.00 |  | 0.94 | 1.00 |  | 1.00 |
| Lane Grp Cap(c), veh/h | 390 | 902 | 886 | 133 | 866 | 895 | 427 | 0 | 410 | 275 | 0 | 253 |
| V/C Ratio(X) | 0.11 | 0.98 | 1.03 | 0.23 | 0.39 | 0.40 | 0.79 | 0.00 | 0.31 | 0.05 | 0.00 | 0.07 |
| Avail Cap(c_a), veh/h | 420 | 902 | 886 | 179 | 878 | 907 | 427 | 0 | 410 | 275 | 0 | 253 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 8.8 | 19.2 | 19.8 | 21.0 | 11.7 | 11.7 | 32.0 | 0.0 | 24.9 | 27.7 | 0.0 | 23.2 |
| Incr Delay (d2), s/veh | 0.1 | 24.4 | 37.1 | 0.9 | 0.3 | 0.3 | 13.8 | 0.0 | 2.0 | 0.1 | 0.0 | 0.1 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 0.5 | 26.7 | 30.3 | 0.4 | 4.8 | 5.0 | 9.7 | 0.0 | 2.7 | 0.3 | 0.0 | 0.3 |
| LnGrp Delay(d),s/veh | 8.9 | 43.7 | 56.9 | 21.9 | 12.0 | 12.0 | 45.8 | 0.0 | 26.9 | 27.7 | 0.0 | 23.4 |
| LnGrp LOS | A | D | F | C | B | B | D |  | C | C |  | C |
| Approach Vol, veh/h |  | 1835 |  |  | 727 |  |  | 464 |  |  | 31 |  |
| Approach Delay, s/veh |  | 49.4 |  |  | 12.4 |  |  | 40.6 |  |  | 25.2 |  |
| Approach LOS |  | D |  |  | B |  |  | D |  |  | C |  |


| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Assigned Phs | 2 | 3 | 4 | 6 | 7 | 8 |  |  |
| Phs Duration (G+Y+Rc), s | 28.4 | 7.1 | 52.0 | 28.4 | 7.8 | 51.4 |  |  |
| Change Period (Y+Rc), s | 4.0 | 4.5 | 4.0 | 4.0 | 4.5 | 4.0 |  |  |
| Max Green Setting (Gmax), s | 24.4 | 5.1 | 48.0 | 24.4 | 5.1 | 48.0 |  |  |
| Max Q Clear Time (g_c+11), s | 25.7 | 2.7 | 50.0 | 9.0 | 3.2 | 12.9 |  |  |
| Green Ext Time (p_c), s | 0.0 | 0.0 | 0.0 | 1.9 | 0.0 | 26.2 |  |  |

Intersection Summary
HCM 2010 Ctrl Delay
39.0

HCM 2010 LOS

|  | 4 |  | \％ | 7 |  | 4 | 4 | $\dagger$ | $p$ | $t$ | $\frac{1}{1}$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{* 17}$ | 4 | 「 | ${ }^{7}$ | 4 | 「 | \％ | 中 ${ }^{\text {a }}$ |  | ${ }^{7}$ | 44 | 「 |
| Volume（veh／h） | 208 | 79 | 247 | 68 | 144 | 47 | 270 | 475 | 36 | 59 | 680 | 291 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q（Qb），veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow，veh／h／ln | 1759 | 1776 | 1863 | 1900 | 1900 | 1759 | 1845 | 1873 | 1900 | 1743 | 1900 | 1810 |
| Adj Flow Rate，veh／h | 270 | 103 | 321 | 113 | 240 | 78 | 314 | 552 | 42 | 72 | 829 | 355 |
| Adj No．of Lanes | 2 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 0 | 1 | 2 | 1 |
| Peak Hour Factor | 0.77 | 0.77 | 0.77 | 0.60 | 0.60 | 0.60 | 0.86 | 0.86 | 0.86 | 0.82 | 0.82 | 0.82 |
| Percent Heavy Veh，\％ | 8 | 7 | 2 | 0 | 0 | 8 | 3 | 1 | 1 | 9 | 0 | 5 |
| Cap，veh／h | 728 | 409 | 365 | 431 | 396 | 312 | 408 | 1181 | 90 | 91 | 1011 | 431 |
| Arrive On Green | 0.10 | 0.23 | 0.23 | 0.08 | 0.21 | 0.21 | 0.12 | 0.35 | 0.35 | 0.05 | 0.28 | 0.28 |
| Sat Flow，veh／h | 3250 | 1776 | 1583 | 1810 | 1900 | 1495 | 3408 | 3353 | 255 | 1660 | 3610 | 1538 |
| Grp Volume（v），veh／h | 270 | 103 | 321 | 113 | 240 | 78 | 314 | 292 | 302 | 72 | 829 | 355 |
| Grp Sat Flow（s），veh／h／ln | 1625 | 1776 | 1583 | 1810 | 1900 | 1495 | 1704 | 1780 | 1828 | 1660 | 1805 | 1538 |
| Q Serve（g＿s），s | 4.2 | 3.2 | 13.2 | 3.2 | 7.7 | 2.9 | 6.0 | 8.6 | 8.6 | 2.9 | 14.4 | 14.5 |
| Cycle Q Clear（g＿c），s | 4.2 | 3.2 | 13.2 | 3.2 | 7.7 | 2.9 | 6.0 | 8.6 | 8.6 | 2.9 | 14.4 | 14.5 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.14 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 728 | 409 | 365 | 431 | 396 | 312 | 408 | 627 | 644 | 91 | 1011 | 431 |
| V／C Ratio（X） | 0.37 | 0.25 | 0.88 | 0.26 | 0.61 | 0.25 | 0.77 | 0.47 | 0.47 | 0.79 | 0.82 | 0.82 |
| Avail Cap（c＿a），veh／h | 1169 | 422 | 377 | 717 | 452 | 356 | 431 | 627 | 644 | 148 | 1073 | 457 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 18.0 | 21.1 | 25.0 | 18.2 | 24.1 | 22.2 | 28.7 | 16.9 | 16.9 | 31.4 | 22.6 | 22.7 |
| Incr Delay（d2），s／veh | 0.3 | 0.3 | 20.1 | 0.3 | 1.8 | 0.4 | 7.9 | 2.5 | 2.4 | 13.9 | 4.9 | 11.1 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 1.9 | 1.6 | 7.7 | 1.6 | 4.2 | 1.2 | 3.3 | 4.6 | 4.8 | 1.7 | 7.8 | 7.5 |
| LnGrp Delay（d），s／veh | 18.3 | 21.5 | 45.1 | 18.5 | 26.0 | 22.7 | 36.6 | 19.4 | 19.3 | 45.3 | 27.5 | 33.8 |
| LnGrp LOS | B | C | D | B | C | C | D | B | B | D | C | C |
| Approach Vol，veh／h |  | 694 |  |  | 431 |  |  | 908 |  |  | 1256 |  |
| Approach Delay，s／veh |  | 31.2 |  |  | 23.4 |  |  | 25.3 |  |  | 30.3 |  |
| Approach LOS |  | C |  |  | C |  |  | C |  |  | C |  |
| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |  |  |  |  |
| Phs Duration（ $G+Y+R c$ ），$s$ | 8.7 | 28.7 | 9.9 | 20.0 | 13.5 | 23.8 | 11.4 | 18.5 |  |  |  |  |
| Change Period（Y＋Rc），s | 5.0 | 5.0 | 4.5 | 4.5 | 5.5 | 5.0 | 4.5 | 4.5 |  |  |  |  |
| Max Green Setting（Gmax），s | 6.0 | 23.0 | 16.0 | 16.0 | 8.5 | 20.0 | 16.0 | 16.0 |  |  |  |  |
| Max Q Clear Time（g＿c＋l1），s | 4.9 | 10.6 | 5.2 | 15.2 | 8.0 | 16.5 | 6.2 | 9.7 |  |  |  |  |
| Green Ext Time（p＿c），s | 0.0 | 7.5 | 0.2 | 0.4 | 0.1 | 2.3 | 0.7 | 2.0 |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM 2010 Ctrl Delay |  |  | 28.2 |  |  |  |  |  |  |  |  |  |
| HCM 2010 LOS |  |  | C |  |  |  |  |  |  |  |  |  |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | 性 |  | ${ }^{7}$ | 性 |  | 7 | F |  | 7 | $\hat{F}$ |  |
| Volume (veh/h) | 55 | 816 | 75 | 73 | 1041 | 68 | 87 | 8 | 64 | 137 | 17 | 126 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial Q (Qb), veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped-Bike Adj(A_pbT) | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus, Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow, veh/h/ln | 1538 | 1692 | 1800 | 1800 | 1691 | 1800 | 1800 | 1784 | 1800 | 1513 | 1590 | 1800 |
| Adj Flow Rate, veh/h | 56 | 833 | 77 | 75 | 1073 | 70 | 98 | 9 | 72 | 144 | 18 | 133 |
| Adj No. of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 0.98 | 0.98 | 0.98 | 0.97 | 0.97 | 0.97 | 0.89 | 0.89 | 0.89 | 0.95 | 0.95 | 0.95 |
| Percent Heavy Veh, \% | 17 | 7 | 7 | 0 | 6 | 6 | 0 | 0 | 0 | 19 | 0 | 0 |
| Cap, veh/h | 151 | 1221 | 113 | 220 | 1257 | 82 | 433 | 43 | 346 | 213 | 24 | 179 |
| Arrive On Green | 0.41 | 0.41 | 0.41 | 0.41 | 0.41 | 0.41 | 0.25 | 0.25 | 0.25 | 0.15 | 0.15 | 0.15 |
| Sat Flow, veh/h | 405 | 2975 | 275 | 590 | 3063 | 200 | 1714 | 171 | 1371 | 1441 | 164 | 1212 |
| Grp Volume(v), veh/h | 56 | 450 | 460 | 75 | 563 | 580 | 98 | 0 | 81 | 144 | 0 | 151 |
| Grp Sat Flow(s),veh/h/ln | 405 | 1607 | 1643 | 590 | 1607 | 1656 | 1714 | 0 | 1542 | 1441 | 0 | 1376 |
| Q Serve(g_s), s | 5.8 | 14.5 | 14.5 | 7.6 | 20.1 | 20.2 | 2.9 | 0.0 | 2.6 | 6.0 | 0.0 | 6.7 |
| Cycle Q Clear(g_c), s | 26.0 | 14.5 | 14.5 | 22.1 | 20.1 | 20.2 | 2.9 | 0.0 | 2.6 | 6.0 | 0.0 | 6.7 |
| Prop In Lane | 1.00 |  | 0.17 | 1.00 |  | 0.12 | 1.00 |  | 0.89 | 1.00 |  | 0.88 |
| Lane Grp Cap(c), veh/h | 151 | 659 | 674 | 220 | 659 | 679 | 433 | 0 | 389 | 213 | 0 | 203 |
| V/C Ratio(X) | 0.37 | 0.68 | 0.68 | 0.34 | 0.85 | 0.85 | 0.23 | 0.00 | 0.21 | 0.68 | 0.00 | 0.74 |
| Avail Cap(c_a), veh/h | 151 | 659 | 674 | 220 | 659 | 679 | 433 | 0 | 389 | 364 | 0 | 347 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter(1) | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay (d), s/veh | 29.7 | 15.3 | 15.3 | 24.4 | 17.0 | 17.0 | 18.8 | 0.0 | 18.7 | 25.6 | 0.0 | 25.8 |
| Incr Delay (d2), s/veh | 1.5 | 2.9 | 2.8 | 0.9 | 10.6 | 10.3 | 1.2 | 0.0 | 1.2 | 3.7 | 0.0 | 5.3 |
| Initial Q Delay(d3),s/veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \%ile BackOfQ(50\%),veh/ln | 1.0 | 6.9 | 7.0 | 1.3 | 10.8 | 11.1 | 1.5 | 0.0 | 1.2 | 2.6 | 0.0 | 2.8 |
| LnGrp Delay(d),s/veh | 31.3 | 18.2 | 18.1 | 25.3 | 27.5 | 27.3 | 20.0 | 0.0 | 19.9 | 29.3 | 0.0 | 31.1 |
| LnGrp LOS | C | B | B | C | C | C | B |  | B | C |  | C |
| Approach Vol, veh/h |  | 966 |  |  | 1218 |  |  | 179 |  |  | 295 |  |
| Approach Delay, s/veh |  | 18.9 |  |  | 27.3 |  |  | 19.9 |  |  | 30.2 |  |
| Approach LOS |  | B |  |  | C |  |  | B |  |  | C |  |


| Timer | 1 | 2 | 3 | 4 | 5 | 6 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |


| Movement | SEL | SET | SER | NWL | NWT | NWR | NEL | NET | NER | SWL | SWT | SWR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{1}$ | 个 ${ }_{\text {P }}$ |  | ${ }^{7}$ | 个觡 |  | ${ }^{1}$ | $\hat{F}$ |  | ${ }^{7}$ | $\hat{\beta}$ |  |
| Volume（veh／h） | 43 | 775 | 200 | 65 | 962 | 43 | 209 | 7 | 64 | 70 | 8 | 84 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow，veh／h／ln | 1417 | 1708 | 1800 | 1607 | 1665 | 1800 | 1731 | 1500 | 1800 | 1161 | 1277 | 1800 |
| Adj Flow Rate，veh／h | 45 | 816 | 211 | 76 | 1132 | 51 | 255 | 9 | 78 | 101 | 12 | 122 |
| Adj No．of Lanes | 1 | 2 | 0 | 1 | 2 | 0 | 1 | 1 | 0 | 1 | 1 | 0 |
| Peak Hour Factor | 0.95 | 0.95 | 0.95 | 0.85 | 0.85 | 0.85 | 0.82 | 0.82 | 0.82 | 0.69 | 0.69 | 0.69 |
| Percent Heavy Veh，\％ | 27 | 6 | 6 | 12 | 6 | 6 | 4 | 20 | 20 | 55 | 0 | 0 |
| Cap，veh／h | 232 | 1098 | 284 | 297 | 1378 | 62 | 347 | 39 | 335 | 320 | 28 | 289 |
| Arrive On Green | 0.04 | 0.43 | 0.43 | 0.06 | 0.45 | 0.45 | 0.29 | 0.29 | 0.29 | 0.29 | 0.29 | 0.29 |
| Sat Flow，veh／h | 1350 | 2554 | 660 | 1531 | 3083 | 139 | 1162 | 134 | 1161 | 814 | 99 | 1002 |
| Grp Volume（v），veh／h | 45 | 518 | 509 | 76 | 581 | 602 | 255 | 0 | 87 | 101 | 0 | 134 |
| Grp Sat Flow（s），veh／h／n | 1350 | 1623 | 1592 | 1531 | 1582 | 1640 | 1162 | 0 | 1295 | 814 | 0 | 1100 |
| Q Serve（g＿s），s | 1.0 | 15.2 | 15.2 | 1.5 | 18.2 | 18.3 | 10.8 | 0.0 | 2.9 | 6.1 | 0.0 | 5.6 |
| Cycle Q Clear（g＿c），s | 1.0 | 15.2 | 15.2 | 1.5 | 18.2 | 18.3 | 16.4 | 0.0 | 2.9 | 9.1 | 0.0 | 5.6 |
| Prop In Lane | 1.00 |  | 0.41 | 1.00 |  | 0.08 | 1.00 |  | 0.90 | 1.00 |  | 0.91 |
| Lane Grp Cap（c），veh／h | 232 | 698 | 684 | 297 | 707 | 733 | 347 | 0 | 374 | 320 | 0 | 317 |
| V／C Ratio（X） | 0.19 | 0.74 | 0.74 | 0.26 | 0.82 | 0.82 | 0.73 | 0.00 | 0.23 | 0.32 | 0.00 | 0.42 |
| Avail Cap（c＿a），veh／h | 293 | 737 | 722 | 346 | 724 | 750 | 347 | 0 | 374 | 320 | 0 | 317 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（1） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 0.00 | 1.00 | 1.00 | 0.00 | 1.00 |
| Uniform Delay（d），s／veh | 11.1 | 13.6 | 13.6 | 10.2 | 13.7 | 13.7 | 23.8 | 0.0 | 15.4 | 18.9 | 0.0 | 16.4 |
| Incr Delay（d2），s／veh | 0.4 | 3.9 | 3.9 | 0.4 | 7.4 | 7.2 | 12.9 | 0.0 | 1.5 | 0.6 | 0.0 | 0.9 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 0.4 | 7.5 | 7.4 | 0.6 | 9.4 | 9.7 | 5.1 | 0.0 | 1.2 | 1.4 | 0.0 | 1.8 |
| LnGrp Delay（d），s／veh | 11.5 | 17.4 | 17.5 | 10.6 | 21.1 | 20.9 | 36.7 | 0.0 | 16.9 | 19.4 | 0.0 | 17.3 |
| LnGrp LOS | B | B | B | B | C | C | D |  | B | B |  | B |
| Approach Vol，veh／h |  | 1072 |  |  | 1259 |  |  | 342 |  |  | 235 |  |
| Approach Delay，s／veh |  | 17.2 |  |  | 20.4 |  |  | 31.6 |  |  | 18.2 |  |
| Approach LOS |  | B |  |  | C |  |  | C |  |  | B |  |


| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Assigned Phs | 2 | 3 | 4 | 6 | 7 | 8 |  |  |
| Phs Duration（G＋Y＋Rc），s | 20.4 | 8.0 | 28.4 | 20.4 | 7.0 | 29.4 |  |  |
| Change Period（Y＋Rc），s | 4.0 | 4.5 | 4.0 | 4.0 | 4.5 | 4.0 |  |  |
| Max Green Setting（Gmax），s | 16.4 | 5.3 | 25.8 | 16.4 | 5.1 | 26.0 |  |  |
| Max Q Clear Time（g＿c＋11），s | 18.4 | 3.5 | 17.2 | 11.1 | 3.0 | 20.3 |  |  |
| Green Ext Time（p＿c），s | 0.0 | 0.0 | 7.2 | 1.5 | 0.0 | 5.0 |  |  |

Intersection Summary
HCM 2010 Ctrl Delay
20.4

HCM 2010 LOS
C

|  | $y$ | $\rightarrow$ |  | 7 |  | 4 | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \％${ }^{*}$ | $\uparrow$ | F | ${ }^{7}$ | $\uparrow$ | F | \％${ }^{1 / 1}$ | 个t |  | \％ | 个个 | F |
| Volume（veh／h） | 515 | 160 | 347 | 55 | 129 | 101 | 449 | 692 | 60 | 99 | 651 | 267 |
| Number | 7 | 4 | 14 | 3 | 8 | 18 | 5 | 2 | 12 | 1 | 6 | 16 |
| Initial $\mathrm{Q}(\mathrm{Qb})$ ，veh | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ， | 0 | 0 | 0 |
| Ped－Bike Adj（A＿pbT） | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 |
| Parking Bus，Adj | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Adj Sat Flow，veh／h／ln | 1593 | 1682 | 1765 | 1800 | 1698 | 1579 | 1748 | 1784 | 1800 | 1579 | 1748 | 1538 |
| Adj Flow Rate，veh／h | 592 | 184 | 399 | 73 | 172 | 135 | 541 | 834 | 72 | 110 | 723 | 297 |
| Adj No．of Lanes | 2 | 1 | 1 | 1 | 1 | 1 | 2 | 2 | 0 | 1 | 2 | 1 |
| Peak Hour Factor | 0.87 | 0.87 | 0.87 | 0.75 | 0.75 | 0.75 | 0.83 | 0.83 | 0.83 | 0.90 | 0.90 | 0.90 |
| Percent Heavy Veh，\％ | 13 | 7 | 2 | 0 | 6 | 14 | 3 | 1 | 1 | 14 | 3 | 17 |
| Cap，veh／h | 792 | 437 | 390 | 297 | 223 | 176 | 625 | 1103 | 95 | 142 | 831 | 327 |
| Arrive On Green | 0.19 | 0.26 | 0.26 | 0.06 | 0.13 | 0.13 | 0.19 | 0.35 | 0.35 | 0.09 | 0.25 | 0.25 |
| Sat Flow，veh／h | 2943 | 1682 | 1500 | 1714 | 1698 | 1342 | 3229 | 3157 | 273 | 1504 | 3320 | 1308 |
| Grp Volume（v），veh／h | 592 | 184 | 399 | 73 | 172 | 135 | 541 | 448 | 458 | 110 | 723 | 297 |
| Grp Sat Flow（s），veh／h／n | 1472 | 1682 | 1500 | 1714 | 1698 | 1342 | 1614 | 1694 | 1735 | 1504 | 1660 | 1308 |
| Q Serve（g＿s），s | 13.7 | 7.5 | 12.4 | 3.0 | 8.1 | 6.1 | 13.5 | 19.4 | 19.4 | 5.9 | 17.3 | 10.9 |
| Cycle Q Clear（g＿c），s | 13.7 | 7.5 | 12.4 | 3.0 | 8.1 | 6.1 | 13.5 | 19.4 | 19.4 | 5.9 | 17.3 | 10.9 |
| Prop In Lane | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 0.16 | 1.00 |  | 1.00 |
| Lane Grp Cap（c），veh／h | 792 | 437 | 390 | 297 | 223 | 176 | 625 | 592 | 607 | 142 | 831 | 327 |
| V／C Ratio（X） | 0.75 | 0.42 | 1.02 | 0.25 | 0.77 | 0.77 | 0.87 | 0.76 | 0.76 | 0.78 | 0.87 | 0.91 |
| Avail Cap（c＿a），veh／h | 800 | 437 | 390 | 522 | 327 | 259 | 642 | 592 | 607 | 181 | 880 | 347 |
| HCM Platoon Ratio | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Upstream Filter（I） | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Uniform Delay（d），s／veh | 23.1 | 25.5 | 10.2 | 28.3 | 34.9 | 19.7 | 32.4 | 23.9 | 23.9 | 36.7 | 29.8 | 10.6 |
| Incr Delay（d2），s／veh | 3.9 | 0.6 | 51.6 | 0.4 | 6.6 | 7.9 | 11.7 | 8.7 | 8.5 | 14.7 | 9.0 | 25.8 |
| Initial Q Delay（d3），s／veh | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \％ile BackOfQ（50\％），veh／ln | 5.9 | 3.6 | 10.7 | 1.4 | 4.2 | 2.6 | 7.0 | 10.5 | 10.7 | 3.1 | 9.0 | 6.2 |
| LnGrp Delay（d），s／veh | 27.0 | 26.2 | 61.8 | 28.7 | 41.5 | 27.6 | 44.1 | 32.6 | 32.4 | 51.4 | 38.9 | 36.5 |
| LnGrp LOS | C | C | F | C | D | C | D | C | C | D | D | D |
| Approach Vol，veh／h |  | 1175 |  |  | 380 |  |  | 1447 |  |  | 1130 |  |
| Approach Delay，s／veh |  | 38.7 |  |  | 34.1 |  |  | 36.8 |  |  | 39.4 |  |
| Approach LOS |  | D |  |  | C |  |  | D |  |  | D |  |


| Timer | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Assigned Phs | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 |
| Phs Duration（G＋Y＋Rc），s | 13.3 | 34.0 | 9.6 | 26.1 | 21.6 | 25.8 | 20.3 | 15.4 |
| Change Period（Y＋Rc），s | 5.5 | $* 5$ | 4.5 | 4.5 | 5.5 | 5.0 | 4.5 | 4.5 |
| Max Green Setting（Gmax），s | 10.0 | $* 29$ | 16.0 | 16.0 | 16.5 | 22.0 | 16.0 | 16.0 |
| Max Q Clear Time（g＿c | （1）），s | 7.9 | 21.4 | 5.0 | 14.4 | 15.5 | 19.3 | 15.7 |
| Green Ext Time（p＿c），s | 0.6 | 3.1 | 0.1 | 0.7 | 0.3 | 1.4 | 0.1 | 0.1 |

Intersection Summary

HCM 2010 Ctrl Delay

37.8

HCM 2010 LOS

D

## Notes

＊HCM 2010 computational engine requires equal clearance times for the phases crossing the barrier．

## Appendix C

## Drainage Support

CALLE SONORA WSEL COMPARISON
HEC-RAS Locations: User Defined Profile: 100-yr

| River | Reach | River Sta | Profile | Plan | Vel Total | W.S. Elev |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | (ft/s) | (ft) |
| Nogales Wash | 1 | 7.204 | 100-yr | CS_BB_BO | 5.85 | 3749.97 |
| Nogales Wash | 1 | 7.198 BR U | 100-yr | Mod_Existing | 6.31 | 3750.25 |
| Nogales Wash | 1 | 7.198 BR U | 100-yr | CS_BB_BO | 6.67 | 3749.97 |
| Nogales Wash | 1 | 7.198 BR D | 100-yr | Mod_Existing | 6.34 | 3749.17 |
| Nogales Wash | 1 | 7.198 BR D | 100-yr | CS_BB_BO | 6.02 | 3748.66 |
| Nogales Wash | 1 | 7.187 | 100-yr | CS_BB_BO | 8.65 | 3747.74 |

CALLE SONORA WSEL COMPARISON


## GOLD HILL RD WSEL COMPARISON

HEC-RAS Locations: User Defined Profile: 100-yr
HEC-RAS Locations: User Defined Profile: 100-yr

| River | Reach | River Sta | Profile | Plan | Vel Total | W.S. Elev |
| :--- | :--- | :--- | :--- | :--- | ---: | :---: |
|  |  |  |  |  | $(\mathrm{ft} / \mathrm{s})$ | $(\mathrm{ft})$ |
| Nogales Wash | 1 | 5.594 | $100-\mathrm{yr}$ | GH_BB_BO | 9.66 | 3687.38 |
|  |  |  |  |  |  |  |
| Nogales Wash | 1 | 5.58 | BR U | $100-\mathrm{yr}$ | Mod_Existing | 9.34 |
| Nogales Wash | 1 | 5.58 | BR U | $100-\mathrm{yr}$ | GH_BB_BO | 9687.57 |
|  |  |  |  |  |  | 9.41 |
| Nogales Wash | 1 | 5.58 | BR D | $100-\mathrm{yr}$ | Mod_Existing | 10.29 |
| Nogales Wash | 1 | 5.58 | BR D | $100-\mathrm{yr}$ | GH_BB_BO | 9687.38 |
|  |  |  |  |  | 9.03 | 3687.38 |
| Nogales Wash | 1 | 5.572 | $100-\mathrm{yr}$ | Mod_Existing | 14.43 | 3683.60 |
| Nogales Wash | 1 | 5.572 | $100-\mathrm{yr}$ | GH_BB_BO | 12.58 | 3684.21 |

GOLD HILL RD WSEL COMPARISON


PRODUCE ROW WSEL COMPARISON

HEC-RAS Locations: User Defined Profile: 100-yr

| River | Reach | River Sta | Profile | Plan | Vel Total | W.S. Elev |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | (ft/s) | (ft) |
| Nogales Wash | 1 | 6.12 | 100-yr | Mod_Existing | 5.47 | 3709.45 |
| Nogales Wash | 1 | 6.12 | 100-yr | PR_AASHTO2_BO | 5.58 | 3708.80 |
| Nogales Wash | 1 | 6.113 BRU | 100-yr | Mod_Existing | 5.89 | 3709.45 |
| Nogales Wash | 1 | 6.113 BR U | 100-yr | PR_AASHTO2_BO | 5.97 | 3708.80 |
| Nogales Wash | 1 | 6.113 BR D | 100-yr | Mod_Existing | 5.43 | 3707.67 |
| Nogales Wash | 1 | 6.113 BRD | 100-yr | PR_AASHTO2_BO | 5.45 | 3707.11 |
| Nogales Wash | 1 | 6.104 | 100-yr | PR_AASHTO2_BO | 9.40 | 3706.93 |

PRODUCE ROW WSEL COMPARISON


## EQUATION 6.3, Standards Manual for Drainage Design and Floodplain Management

## Nogales Wash - Calle Sonora Bridge

$\mathrm{Z}_{\mathrm{t}}=\quad$ Design scour depth, excluding long-term aggradation/degradation, in feet;
$\mathrm{Z}_{\mathrm{gs}}=\quad$ General scour depth, in feet;
$\mathrm{Z}_{\mathrm{a}}=\quad$ Anti-dune trough depth, in feet;
$Z_{\text {Is }}=\quad$ Local scour depth, in feet;
$Z_{b s}=\quad$ Bend scour depth, in feet;
$\mathrm{Z}_{\mathrm{fft}}=\quad$ Low-flow thalweg depth, in feet;
$\mathrm{Z}_{\mathrm{t}}=\quad \mathbf{1 . 3} *\left(\mathrm{Z}_{\mathrm{gs}}+\mathbf{1 / 2} \mathrm{Z}_{\mathrm{a}}+\mathrm{Z}_{\mathrm{ls}}+\mathrm{Z}_{\mathrm{bs}}+\mathrm{Z}_{\mathrm{fft}}\right)$

| $\mathrm{Z}_{\mathrm{gs}}=$ | 4.7 ft |
| :---: | :---: |
| $\mathrm{Z}_{\mathrm{a}}=$ | 2.5 f |
| $\mathrm{Z}_{\text {lsp }}=$ | 9.9 ft |
| $\mathrm{Z}_{\text {Ise }}$ | 0.0 |
| $\mathrm{Z}_{\mathrm{bs}}=$ | 0.0 ft |
| $\mathrm{Z}_{\mathrm{lft}}=$ | 2.0 ft |
| $\mathrm{Z}_{\text {lss }}=$ | 0.0 |

$$
\mathrm{Z}_{\mathrm{t}}=\quad 23.2 \mathrm{ft}
$$

## EQUATION 6.4, Standards Manual for Drainage Design

and Floodplain Management
$\mathrm{Z}_{\mathrm{gs}}=\quad$ General scour depth, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$\mathrm{Y}_{\text {max }}=\quad$ Maximum depth of flow, in feet;
$\mathrm{Y}_{\mathrm{h}}=\quad$ Hydraulic depth of flow, in feet;
$\mathrm{S}_{\mathrm{e}}=\quad$ Energy slope ( or bed slope for uniform-flow conditions), in feet per foot
$\mathrm{Z}_{\mathrm{g} s}=\quad Y_{\max }\left[\left(0.0685 \mathrm{~V}_{\mathrm{m}}^{0.8} / \mathrm{Y}_{\mathrm{h}}^{0.4} \mathrm{~S}_{\mathrm{e}}^{0.3}\right)_{-1}\right]$

| $\mathrm{V}_{\mathrm{m}}=$ | 13.52 | fps |
| :--- | ---: | ---: |
| $\mathrm{Y}_{\text {max }}=$ | 12.59 | ft |
| $\mathrm{Y}_{\mathrm{h}}=$ | 12.59 | ft |
| $\mathrm{S}_{\mathrm{e}}=$ | 0.001631 | $\mathrm{ft} / \mathrm{ft}$ |

$$
\mathrm{Z}_{\mathrm{gs}}=\quad 4.658 \mathrm{ft}
$$

**Hydraulics from XS 7.204

## EQUATION 6.5, Standards Manual for Drainage Design and Floodplain Management

$\mathrm{Z}_{\mathrm{a}}=\quad$ Anti-dune trough depth, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$\mathrm{g}=\quad$ Acceleration due to gravity, in feet per second squared;
$\mathrm{Z}_{\mathrm{a}}=\quad \mathbf{0 . 5 ( 0 . 1 4 ) 2 q [ \mathrm { V } _ { \mathrm { m } } { } ^ { 2 } / \mathrm { g } = 0 . 0 1 3 7 \mathrm { V } _ { \mathrm { m } } { } ^ { 2 } { } ^ { 2 } , ~}$
$\mathrm{V}_{\mathrm{m}}=$
13.52 fps
$\mathrm{g}=\quad 32.2 \mathrm{ft} / \mathrm{sec}^{2}$

**Hydraulics from XS 7.204

## Section 6.6.3, Standards Manual for Drainage Design and Floodplain Management

$Z_{\mathrm{lft}}=\quad$ Low flow thalweg depth, in feet;
$\mathrm{Y}=\quad$ Flow depth; in feet;
$\mathrm{W}=\quad$ Flow width; in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average Velocity of flow, in feet per second;
$\mathrm{Z}_{\mathrm{lft}}=\quad 1$ when $\mathrm{W} / \mathrm{Y}>1.15 \mathrm{~V}_{\mathrm{m}}$

| $\mathrm{V}_{\mathrm{m}}=$ | 13.52 fps |
| :--- | ---: |
| $\mathrm{W}=$ | 1726.49 ft |
| $\mathrm{Y}=$ | 12.6 ft |
| $\mathrm{W} / \mathrm{Y}=$ | 137.1 |
| $1.15 \mathrm{~V}_{\mathrm{m}}=$ | $\mathbf{1 5 . 5}$ |
|  |  |

Regional or Non-Reg Regional

## Section 6.6.4, Standards Manual for Drainage Design and Floodplain Management

$\mathrm{Z}_{\mathrm{lft}}=\quad$ Bend scour component, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$Y_{\max }=\quad$ Maximum depth of flow immediately upstream of bend, in feet;
$\mathrm{Y}_{\mathrm{h}}=\quad$ Hydraulic depth of flow immediately upstream of bend, in feet;
$\mathrm{S}_{\mathrm{e}}=\quad$ Energy slope ( or bed slope for uniform-flow conditions), in feet per foot
$\alpha=\quad$ Angle between centerline of channel and outside bend tangent line, in degrees
$Z_{b s}=\quad\left(0.0685 Y_{\max } V_{m}{ }^{0.8} / Y_{h}{ }^{0.4} S_{e}{ }^{0.3}\right)\left[2.1\left(\sin ^{2}(\alpha / 2) / \cos \alpha\right)^{0.2}-1\right]$

| $\mathrm{V}_{\mathrm{m}}=$ | 13.52 fps |
| :---: | :---: |
| $\mathrm{Y}_{\text {max }}=$ | 12.59 ft |
| $\mathrm{Y}_{\mathrm{h}}=$ | 12.59 ft |
| $\mathrm{S}_{\mathrm{e}}=$ | $0.001631 \mathrm{ft} / \mathrm{ft}$ |
| $\alpha=$ | 0 degrees |
| $\alpha=$ | 0.00 radians |

$$
\mathrm{Z}_{\mathrm{bs}}=\quad 0.00 \mathrm{ft}
$$

**Hydraulics from XS 7.204

## Section 6.6.5, Standards Manual for Drainage Design and Floodplain Management

$Z_{\text {lsp }}=\quad$ Local scour due to piers, in feet
$\mathrm{Y}=\quad$ Flow depth, in feet
$\mathrm{b}_{\mathrm{p}}=\quad$ Pier width normal to flow direction, in feet
$\mathrm{F}_{\mathrm{u}}=\quad$ Upstream Froude number
$\mathrm{R}_{\mathrm{f}}=\quad$ Reduction Factor (Table 6.1)
$Z_{\text {lsp }}=\quad \mathbf{2 . 2} \mathbf{R}_{\mathbf{f}} \mathbf{Y}\left[\left(\mathbf{b}_{\mathrm{p}} / \mathbf{Y}\right)^{\mathbf{0 . 6 5}}\right] \mathbf{F}_{\mathbf{u}}^{\mathbf{0 . 4 3}}$
$b_{p e}=\quad$ Effective pier width, in feet
$\mathrm{L}=\quad$ Length of pier wall, in feet
$\phi_{\mathrm{p}}=\quad$ Angle of approach flow in relationship to pier wall, in degrees
$b_{p e}=\quad L \sin \emptyset_{p}+b_{p} \cos \emptyset_{p}$

| $\mathrm{Y}=$ | 13.82 ft |
| :---: | :---: |
| $\mathrm{b}_{\mathrm{p}}=$ | 5 ft |
| $\mathrm{F}_{\mathrm{u}}=$ | 0.44 |
| $\mathrm{R}_{\mathrm{f}}=$ | 0.9 |
| $\mathrm{b}_{\mathrm{pe}}=$ | 5.00 |
| $\mathrm{L}=$ | 69.75 |
| $\phi_{\mathrm{p}}=$ | 0 degrees |
| $\phi_{\mathrm{p}}=$ | 0.00 radians |


**Hydraulics from downstream Internal Bridge Cross-Section

## EQUATION 6.3, Standards Manual for Drainage Design and Floodplain Management

## Nogales Wash - Calle Sonora Bridge 10-Year

$\mathrm{Z}_{\mathrm{t}}=\quad$ Design scour depth, excluding long-term aggradation/degradation, in feet;
$\mathrm{Z}_{\mathrm{gs}}=\quad$ General scour depth, in feet;
$\mathrm{Z}_{\mathrm{a}}=\quad$ Anti-dune trough depth, in feet;
$Z_{\text {Is }}=\quad$ Local scour depth, in feet;
$Z_{b s}=\quad$ Bend scour depth, in feet;
$\mathrm{Z}_{\mathrm{fft}}=\quad$ Low-flow thalweg depth, in feet;
$\mathrm{Z}_{\mathrm{t}}=\quad \mathbf{1 . 3} *\left(\mathrm{Z}_{\mathrm{gs}}+\mathbf{1 / 2} \mathrm{Z}_{\mathrm{a}}+\mathrm{Z}_{\mathrm{ls}}+\mathrm{Z}_{\mathrm{bs}}+\mathrm{Z}_{\mathrm{fft}}\right)$

| $\mathrm{Z}_{\mathrm{gs}}=$ | 0.0 ft |
| :---: | :---: |
| $\mathrm{Z}_{\mathrm{a}}=$ | 0.4 f |
| $\mathrm{Z}_{\text {lsp }}=$ | 9.9 ft |
| $\mathrm{Z}_{\text {Ise }}$ | 0.0 |
| $\mathrm{Z}_{\mathrm{bs}}=$ | 0.0 ft |
| $\mathrm{Z}_{\mathrm{lft}}=$ | 2.0 ft |
| $\mathrm{Z}_{\text {lss }}=$ | 0.0 |



## EQUATION 6.4, Standards Manual for Drainage Design

and Floodplain Management

Nogales W General scour depth, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$\mathrm{Y}_{\text {max }}=\quad$ Maximum depth of flow, in feet;
$\mathrm{Y}_{\mathrm{h}}=\quad$ Hydraulic depth of flow, in feet;
$S_{e}=\quad$ Energy slope ( or bed slope for uniform-flow conditions), in feet per foot
$\mathrm{Z}_{\mathrm{g} s}=\quad Y_{\max }\left[\left(0.0685 \mathrm{~V}_{\mathrm{m}}^{0.8} / \mathrm{Y}_{\mathrm{h}}^{0.4} \mathrm{~S}_{\mathrm{e}}^{0.3}\right)_{-1}\right]$

| $\mathrm{V}_{\mathrm{m}}=$ | 5.3 fps |
| :--- | ---: |
| $\mathrm{Y}_{\text {max }}=$ | 9.5 ft |
| $\mathrm{Y}_{\mathrm{h}}=$ | 9.5 ft |
| $\mathrm{S}_{\mathrm{e}}=$ | 0.000667 |
| $\mathrm{ft} / \mathrm{ft}$ |  |

$$
\mathrm{Z}_{\mathrm{gs}}=\quad 0.000 \mathrm{ft}
$$

**Hydraulics from XS 7.204

## EQUATION 6.5, Standards Manual for Drainage Design and Floodplain Management

Nogales W Anti-dune trough depth, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$\mathrm{g}=\quad$ Acceleration due to gravity, in feet per second squared;
$\mathrm{Z}_{\mathrm{a}}=\quad \mathbf{0 . 5 ( 0 . 1 4 )} 2 \Psi \mathrm{~V}_{\mathrm{m}}{ }^{2} / \mathrm{g}=\mathbf{0 . 0 1 3 7} \mathrm{V}_{\mathrm{m}}{ }^{2}$
$\mathrm{V}_{\mathrm{m}}=$
5.3 fps
$\mathrm{g}=\quad 32.2 \mathrm{ft} / \mathrm{sec}^{2}$

**Hydraulics from XS 7.204

## Section 6.6.3, Standards Manual for Drainage Design and Floodplain Management

Nogales W Low flow thalweg depth, in feet;
$\mathrm{Y}=\quad$ Flow depth; in feet;
$\mathrm{W}=\quad$ Flow width; in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average Velocity of flow, in feet per second;
$\mathrm{Z}_{\mathrm{lft}}=\quad 1$ when $\mathrm{W} / \mathrm{Y}>1.15 \mathrm{~V}_{\mathrm{m}}$

| $\mathrm{V}_{\mathrm{m}}=$ | 5.3 fps |
| :--- | ---: |
| $\mathrm{W}=$ | 1726.49 ft |
| $\mathrm{Y}=$ | 9.5 ft |
| $\mathrm{W} / \mathrm{Y}=$ | 181.7 |
| $1.15 \mathrm{~V}_{\mathrm{m}}=$ | $\mathbf{6 . 1}$ |

Regional or Non-Reg Regional

## Section 6.6.4, Standards Manual for Drainage Design and Floodplain Management

Nogales W Bend scour component, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$Y_{\max }=\quad$ Maximum depth of flow immediately upstream of bend, in feet;
$\mathrm{Y}_{\mathrm{h}}=\quad$ Hydraulic depth of flow immediately upstream of bend, in feet;
$\mathrm{S}_{\mathrm{e}}=\quad$ Energy slope ( or bed slope for uniform-flow conditions), in feet per foot
$\alpha=\quad$ Angle between centerline of channel and outside bend tangent line, in degrees
$Z_{b s}=\quad\left(0.0685 Y_{\max } V_{m}{ }^{0.8} / Y_{h}{ }^{0.4} S_{e}{ }^{0.3}\right)\left[2.1\left(\sin ^{2}(\alpha / 2) / \cos \alpha\right)^{0.2}-1\right]$

| $\mathrm{V}_{\mathrm{m}}=$ | 5.3 fps |
| :---: | :---: |
| $\mathrm{Y}_{\text {max }}=$ | 9.5 ft |
| $\mathrm{Y}_{\mathrm{h}}=$ | 9.5 ft |
| $\mathrm{S}_{\mathrm{e}}=$ | $0.000667 \mathrm{ft} / \mathrm{ft}$ |
| $\alpha=$ | 0 degrees |
| $\alpha=$ | 0.00 radians |

$$
\mathrm{Z}_{\mathrm{bs}}=\quad 0.00 \mathrm{ft}
$$

**Hydraulics from XS 7.204

## Section 6.6.5, Standards Manual for Drainage Design and Floodplain Management

Nogales W Local scour due to piers, in feet
$\mathrm{Y}=\quad$ Flow depth, in feet
$\mathrm{b}_{\mathrm{p}}=\quad$ Pier width normal to flow direction, in feet
$\mathrm{F}_{\mathrm{u}}=\quad$ Upstream Froude number
$\mathrm{R}_{\mathrm{f}}=\quad$ Reduction Factor (Table 6.1)
$Z_{\text {lsp }}=\quad 2.2 \mathbf{R}_{\mathbf{f}} \mathbf{Y}\left[\left(\mathbf{b}_{\mathbf{p}} / \mathbf{Y}\right)^{\mathbf{0 . 6 5}}\right] \mathbf{F}_{\mathbf{u}}{ }^{\mathbf{0 . 4 3}}$
$b_{p e}=\quad$ Effective pier width, in feet
$\mathrm{L}=\quad$ Length of pier wall, in feet
$\phi_{\mathrm{p}}=\quad$ Angle of approach flow in relationship to pier wall, in degrees
$b_{p e}=\quad L \sin \emptyset_{p}+b_{p} \cos \emptyset_{p}$

| $\mathrm{Y}=$ | 13.82 ft |
| :---: | :---: |
| $\mathrm{b}_{\mathrm{p}}=$ | 5 ft |
| $\mathrm{F}_{\mathrm{u}}=$ | 0.44 |
| $\mathrm{R}_{\mathrm{f}}=$ | 0.9 |
| $\mathrm{b}_{\mathrm{pe}}=$ | 5.00 |
| $\mathrm{L}=$ | 69.75 |
| $\phi_{\mathrm{p}}=$ | 0 degrees |
| $\emptyset_{\mathrm{p}}=$ | 0.00 radians |


**Hydraulics from downstream Internal Bridge Cross-Section

## EQUATION 6.3, Standards Manual for Drainage Design and Floodplain Management

## Nogales Wash - Gold Hill Road 10-Year

$\mathrm{Z}_{\mathrm{t}}=\quad$ Design scour depth, excluding long-term aggradation/degradation, in feet;
$\mathrm{Z}_{\mathrm{gs}}=\quad$ General scour depth, in feet;
$\mathrm{Z}_{\mathrm{a}}=\quad$ Anti-dune trough depth, in feet;
$Z_{\text {Is }}=\quad$ Local scour depth, in feet;
$Z_{b s}=\quad$ Bend scour depth, in feet;
$\mathrm{Z}_{\mathrm{fft}}=\quad$ Low-flow thalweg depth, in feet;
$\mathrm{Z}_{\mathrm{t}}=\quad \mathbf{1 . 3} *\left(\mathrm{Z}_{\mathrm{gs}}+\mathbf{1 / 2} \mathrm{Z}_{\mathrm{a}}+\mathrm{Z}_{\mathrm{ls}}+\mathrm{Z}_{\mathrm{bs}}+\mathrm{Z}_{\mathrm{fft}}\right)$

| $\mathrm{Z}_{\mathrm{gs}}=$ | 2.5 ft |
| :---: | :---: |
| $\mathrm{Z}_{\mathrm{a}}=$ | 1.1 ft |
| $\mathrm{Z}_{\text {lsp }}=$ | 0.0 ft |
| $\mathrm{Z}_{\text {Ise }}$ | 0.0 |
| $\mathrm{Z}_{\mathrm{bs}}=$ | 0.0 ft |
| $\mathrm{Z}_{\mathrm{lft}}=$ | 2.0 ft |
| $\mathrm{Z}_{\text {lss }}=$ | 0.0 |

$$
\mathrm{Z}_{\mathrm{t}}=\quad 6.6 \mathrm{ft}
$$

## EQUATION 6.4, Standards Manual for Drainage Design

and Floodplain Management
$\mathrm{Z}_{\mathrm{gs}}=\quad$ General scour depth, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$\mathrm{Y}_{\text {max }}=\quad$ Maximum depth of flow, in feet;
$\mathrm{Y}_{\mathrm{h}}=\quad$ Hydraulic depth of flow, in feet;
$\mathrm{S}_{\mathrm{e}}=\quad$ Energy slope ( or bed slope for uniform-flow conditions), in feet per foot
$Z_{\mathrm{g} s}=\quad Y_{\max }\left[\left(0.0685 \mathrm{~V}_{\mathrm{m}}{ }^{0.8} / \mathrm{Y}_{\mathrm{h}}^{0.4} \mathrm{~S}_{\mathrm{e}}{ }^{0.3}\right)_{-1}\right]$

| $\mathrm{V}_{\mathrm{m}}=$ | 9 fps |
| :--- | ---: |
| $\mathrm{Y}_{\text {max }}=$ | 8.3 ft |
| $\mathrm{Y}_{\mathrm{h}}=$ | 8.3 ft |
| $\mathrm{S}_{\mathrm{e}}=$ | $0.001143 \mathrm{ft} / \mathrm{ft}$ |

$$
\mathrm{Z}_{\mathrm{gs}}=\quad 2.492 \mathrm{ft}
$$

**Hydraulics from XS 5.594

## EQUATION 6.5, Standards Manual for Drainage Design and Floodplain Management

$\mathrm{Z}_{\mathrm{a}}=\quad$ Anti-dune trough depth, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$\mathrm{g}=\quad$ Acceleration due to gravity, in feet per second squared;
$\mathrm{Z}_{\mathrm{a}}=\quad \mathbf{0 . 5 ( 0 . 1 4 ) 2 q [ \mathrm { V } _ { \mathrm { m } } { } ^ { 2 } / \mathrm { g } = 0 . 0 1 3 7 \mathrm { V } _ { \mathrm { m } } { } ^ { 2 } { } ^ { 2 } , ~}$
$\mathrm{V}_{\mathrm{m}}=$
$\underline{9} \mathrm{fps}$
$\mathrm{g}=\quad 32.2 \mathrm{ft} / \mathrm{sec}^{2}$

**Hydraulics from XS 5.594

## Section 6.6.3, Standards Manual for Drainage Design and Floodplain Management

$Z_{\mathrm{lft}}=\quad$ Low flow thalweg depth, in feet;
$\mathrm{Y}=\quad$ Flow depth; in feet;
$\mathrm{W}=\quad$ Flow width; in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average Velocity of flow, in feet per second;
$\mathrm{Z}_{\mathrm{lft}}=\quad 1$ when $\mathrm{W} / \mathrm{Y}>1.15 \mathrm{~V}_{\mathrm{m}}$

| $\mathrm{V}_{\mathrm{m}}=$ | 9 fps |
| :--- | ---: |
| $\mathrm{W}=$ | 1637.05 ft |
| $\mathrm{Y}=$ | 8.3 ft |
| $\mathrm{W} / \mathrm{Y}=$ | 197.2 |
| $1.15 \mathrm{~V}_{\mathrm{m}}=$ | 10.4 |
|  |  |

Regional or Non-Reg Regional

## Section 6.6.4, Standards Manual for Drainage Design and Floodplain Management

$\mathrm{Z}_{\mathrm{lft}}=\quad$ Bend scour component, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$Y_{\max }=\quad$ Maximum depth of flow immediately upstream of bend, in feet;
$\mathrm{Y}_{\mathrm{h}}=\quad$ Hydraulic depth of flow immediately upstream of bend, in feet;
$\mathrm{S}_{\mathrm{e}}=\quad$ Energy slope ( or bed slope for uniform-flow conditions), in feet per foot
$\alpha=\quad$ Angle between centerline of channel and outside bend tangent line, in degrees
$Z_{b s}=\quad\left(0.0685 Y_{\max } V_{m}{ }^{0.8} / Y_{h}{ }^{0.4} S_{e}{ }^{0.3}\right)\left[2.1\left(\sin ^{2}(\alpha / 2) / \cos \alpha\right)^{0.2}-1\right]$

| $\mathrm{V}_{\mathrm{m}}=$ | fps |
| :--- | ---: |
| $\mathrm{Y}_{\text {max }}=$ | 8.3 <br> ft |
| $\mathrm{Y}_{\mathrm{h}}=$ | 8.3 ft |
| $\mathrm{S}_{\mathrm{e}}=$ | $\overline{0.001143} \mathrm{ft} / \mathrm{ft}$ |
| $\alpha=$ | 3 |
| $\alpha=$ | degrees |

$$
\mathrm{Z}_{\mathrm{bs}}=\quad 0.00 \mathrm{ft}
$$

**Hydraulics from XS 5.594

## Section 6.6.5, Standards Manual for Drainage Design and Floodplain Management

$Z_{\text {lsp }}=\quad$ Local scour due to piers, in feet
$\mathrm{Y}=\quad$ Flow depth, in feet
$\mathrm{b}_{\mathrm{p}}=\quad$ Pier width normal to flow direction, in feet
$\mathrm{F}_{\mathrm{u}}=\quad$ Upstream Froude number
$\mathrm{R}_{\mathrm{f}}=\quad$ Reduction Factor (Table 6.1)
$Z_{\text {lsp }}=\quad \mathbf{2 . 2} \mathbf{R}_{\mathrm{f}} \mathbf{Y}\left[\left(\mathbf{b}_{\mathrm{p}} / \mathbf{Y}\right)^{\mathbf{0 . 6 5}}\right] \mathbf{F}_{\mathbf{u}}^{\mathbf{0 . 4 3}}$
$b_{p e}=\quad$ Effective pier width, in feet
$\mathrm{L}=\quad$ Length of pier wall, in feet
$\phi_{\mathrm{p}}=\quad$ Angle of approach flow in relationship to pier wall, in degrees
$b_{p e}=\quad L \sin \emptyset_{p}+b_{p} \cos \emptyset_{p}$

| $\mathrm{Y}=$ | 20.19 ft |
| :---: | :---: |
| $\mathrm{b}_{\mathrm{p}}=$ | 0 ft |
| $\mathrm{F}_{\mathrm{u}}=$ | 0.54 |
| $\mathrm{R}_{\mathrm{f}}=$ | 0.9 |
| $\mathrm{b}_{\mathrm{pe}}=$ | 0.00 |
| $\mathrm{L}=$ | 0 |
| $\phi_{\mathrm{p}}=$ | 0 degrees |
| $\phi_{\mathrm{p}}=$ | 0.00 radians |


**Hydraulics from downstream Internal Bridge Cross-Section

## EQUATION 6.3, Standards Manual for Drainage Design and Floodplain Management

## Nogales Wash - Produce Row Bridge -10Yr

$\mathrm{Z}_{\mathrm{t}}=\quad$ Design scour depth, excluding long-term aggradation/degradation, in feet;
$\mathrm{Z}_{\mathrm{gs}}=\quad$ General scour depth, in feet;
$\mathrm{Z}_{\mathrm{a}}=\quad$ Anti-dune trough depth, in feet;
$Z_{\text {Is }}=\quad$ Local scour depth, in feet;
$Z_{b s}=\quad$ Bend scour depth, in feet;
$\mathrm{Z}_{\mathrm{fft}}=\quad$ Low-flow thalweg depth, in feet;
$\mathrm{Z}_{\mathrm{t}}=\quad \mathbf{1 . 3} *\left(\mathrm{Z}_{\mathrm{gs}}+\mathbf{1 / 2} \mathrm{Z}_{\mathrm{a}}+\mathrm{Z}_{\mathrm{ls}}+\mathrm{Z}_{\mathrm{bs}}+\mathrm{Z}_{\mathrm{fft}}\right)$

| $\mathrm{Z}_{\mathrm{gs}}=$ | 4.1 ft |
| :---: | :---: |
| $\mathrm{Z}_{\mathrm{a}}=$ | 1.3 ft |
| $\mathrm{Z}_{\text {lsp }}=$ | 0.0 ft |
| $\mathrm{Z}_{\text {se }}$ | 0.0 |
| $\mathrm{Z}_{\mathrm{bs}}=$ | 0.0 ft |
| $\mathrm{Z}_{\mathrm{lft}}=$ | 2.0 ft |
| $\mathrm{Z}_{\text {lss }}=$ | 0.0 |

$$
\mathbf{Z}_{\mathrm{t}}=\quad 8.8 \mathrm{ft}
$$

## EQUATION 6.4, Standards Manual for Drainage Design

and Floodplain Management

Nogales W General scour depth, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$\mathrm{Y}_{\text {max }}=\quad$ Maximum depth of flow, in feet;
$\mathrm{Y}_{\mathrm{h}}=\quad$ Hydraulic depth of flow, in feet;
$S_{e}=\quad$ Energy slope ( or bed slope for uniform-flow conditions), in feet per foot
$\mathrm{Z}_{\mathrm{g} s}=\quad Y_{\max }\left[\left(0.0685 \mathrm{~V}_{\mathrm{m}}^{0.8} / \mathrm{Y}_{\mathrm{h}}^{0.4} \mathrm{~S}_{\mathrm{e}}^{0.3}\right)_{-1}\right]$

| $\mathrm{V}_{\mathrm{m}}=$ | 9.7 |
| :---: | :---: |
| $\mathrm{Y}_{\text {max }}=$ | 9.05 |
| $\mathrm{Y}_{\mathrm{h}}=$ | 9.05 |
| $\mathrm{S}_{\mathrm{e}}=$ | 0.000852 |

$$
\mathrm{Z}_{\mathrm{gs}}=\quad 4.132 \mathrm{ft}
$$

**Hydraulics from XS 6.12

## EQUATION 6.5, Standards Manual for Drainage Design and Floodplain Management

Nogales W Anti-dune trough depth, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$\mathrm{g}=\quad$ Acceleration due to gravity, in feet per second squared;
$\mathrm{Z}_{\mathrm{a}}=\quad \mathbf{0 . 5 ( 0 . 1 4 )} 2 \Psi \mathrm{~V}_{\mathrm{m}}{ }^{2} / \mathrm{g}=\mathbf{0 . 0 1 3 7} \mathrm{V}_{\mathrm{m}}{ }^{2}$
$\mathrm{V}_{\mathrm{m}}=$ $\qquad$
$\mathrm{g}=\quad 32.2 \mathrm{ft} / \mathrm{sec}^{2}$

**Hydraulics from XS 6.12

## Section 6.6.3, Standards Manual for Drainage Design and Floodplain Management

Nogales W Low flow thalweg depth, in feet;
$\mathrm{Y}=\quad$ Flow depth; in feet;
$\mathrm{W}=\quad$ Flow width; in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average Velocity of flow, in feet per second;
$\mathrm{Z}_{\mathrm{lft}}=\quad 1$ when $\mathrm{W} / \mathrm{Y}>1.15 \mathrm{~V}_{\mathrm{m}}$

| $\mathrm{V}_{\mathrm{m}}=$ | 9.7 fps |  |  |
| :---: | :---: | :---: | :---: |
| $\mathrm{W}=$ | 569 ft | $\mathrm{Z}_{\mathrm{ift}}=$ | 2.00 |
| $\mathrm{Y}=$ | 9.1 ft |  |  |
| $\mathrm{W} / \mathrm{Y}=$ | 6.9 |  |  |
| $1.15 \mathrm{~V}_{\mathrm{m}}=$ | 11.2 |  |  |

Regional or Non-Reg Regional
**Hydraulics from XS 6.12

## Section 6.6.4, Standards Manual for Drainage Design and Floodplain Management

Nogales W Bend scour component, in feet;
$\mathrm{V}_{\mathrm{m}}=\quad$ Average velocity of flow, in feet per second;
$Y_{\max }=\quad$ Maximum depth of flow immediately upstream of bend, in feet;
$\mathrm{Y}_{\mathrm{h}}=\quad$ Hydraulic depth of flow immediately upstream of bend, in feet;
$\mathrm{S}_{\mathrm{e}}=\quad$ Energy slope ( or bed slope for uniform-flow conditions), in feet per foot
$\alpha=\quad$ Angle between centerline of channel and outside bend tangent line, in degrees
$Z_{b s}=\quad\left(0.0685 Y_{\max } V_{m}{ }^{0.8} / Y_{h}{ }^{0.4} S_{e}{ }^{0.3}\right)\left[2.1\left(\sin ^{2}(\alpha / 2) / \cos \alpha\right)^{0.2}-1\right]$

| $\mathrm{V}_{\mathrm{m}}=$ | 9.7 fps |
| :---: | :---: |
| $\mathrm{Y}_{\text {max }}=$ | 9.05 ft |
| $\mathrm{Y}_{\mathrm{h}}=$ | 9.05 ft |
| $\mathrm{S}_{\mathrm{e}}=$ | $0.000852 \mathrm{ft} / \mathrm{ft}$ |
| $\alpha=$ | 0 degrees |
| $\alpha=$ | 0.00 radians |

$$
\mathrm{Z}_{\mathrm{bs}}=\quad 0.00 \mathrm{ft}
$$

**Hydraulics from XS 6.12

## Section 6.6.5, Standards Manual for Drainage Design and Floodplain Management

Nogales W Local scour due to piers, in feet
$\mathrm{Y}=\quad$ Flow depth, in feet
$\mathrm{b}_{\mathrm{p}}=\quad$ Pier width normal to flow direction, in feet
$\mathrm{F}_{\mathrm{u}}=\quad$ Upstream Froude number
$\mathrm{R}_{\mathrm{f}}=\quad$ Reduction Factor (Table 6.1)
$Z_{\text {lsp }}=\quad 2.2 \mathbf{R}_{\mathbf{f}} \mathbf{Y}\left[\left(\mathbf{b}_{\mathbf{p}} / \mathbf{Y}\right)^{\mathbf{0 . 6 5}}\right] \mathbf{F}_{\mathbf{u}}{ }^{\mathbf{0 . 4 3}}$
$b_{p e}=\quad$ Effective pier width, in feet
$\mathrm{L}=\quad$ Length of pier wall, in feet
$\phi_{\mathrm{p}}=\quad$ Angle of approach flow in relationship to pier wall, in degrees
$b_{p e}=\quad L \sin \emptyset_{p}+b_{p} \cos \emptyset_{p}$

| $\mathrm{Y}=$ | 15.01 ft |
| :---: | :---: |
| $\mathrm{b}_{\mathrm{p}}=$ | 0 ft |
| $\mathrm{F}_{\mathrm{u}}=$ | 0.47 |
| $\mathrm{R}_{\mathrm{f}}=$ | 0.9 |
| $\mathrm{b}_{\mathrm{pe}}=$ | 0.00 |
| $\mathrm{L}=$ | 0 |
| $\phi_{\mathrm{p}}=$ | 0 degrees |
| $\phi_{\mathrm{p}}=$ | 0.00 radians |


**Hydraulics from downstream Internal Bridge Cross-Section

